

# WASHINGTON COUNTY, OREGON AND INCORPORATED AREAS

# VOLUME 1 OF 3

COMMUNITY	
NAME	

COMMUNITY NUMBER

410238

BANKS, CITY OF
BEAVERTON, CITY OF
CORNELIUS, CITY OF
DURHAM, CITY OF
FOREST GROVE, CITY OF
GASTON, CITY OF
HILLSBORO, CITY OF
KING CITY, CITY OF
NORTH PLAINS, CITY OF
SHERWOOD, CITY OF
TIGARD, CITY OF
TUALATIN, CITY OF
WASHINGTON COUNTY
UNINCORPORATED AREAS



Effective: November 4, 2016



Federal Emergency Management Agency Flood Insurance Study Number 41067CV001A

#### NOTICE TO

#### FLOOD INSURANCE STUDY USERS

Communities participating in the National Flood Insurance Program have established repositories of flood hazard data for floodplain management and flood insurance purposes. This Flood Insurance Study (FIS) may not contain all data available within the repository. It is advisable to contact the community repository for any additional data.

Selected Flood Insurance Rate Map panels for the community contain information that was previously shown separately on the corresponding Flood Boundary and Floodway Map panels (e.g., floodways, cross sections). In addition, former flood hazard zone designations have been changed as follows:

<u>Old Zone</u>	<u>New Zone</u>
A1 through A30	AE
V1 through V30	VE
В	Х
С	Х

Part or all of this FIS may be revised and republished at any time. In addition, part of this FIS may be revised by a Letter of Map Revision process, which does not involve republication or redistribution of the FIS. It is, therefore, the responsibility of the user to consult with community officials and to check the community repository to obtain the most current FIS report components.

Users should refer to Section 10.0, Revisions Descriptions. Section 10.0 is intended to present the most up-to-date information for specific portions of this FIS report. Therefore, users of this FIS report should be aware that the information presented in Section 10.0 supersedes information in Sections 1.0 through 9.0 of this FIS report.

Initial Countywide FIS Effective Date: November 4, 2016

**Revised FIS Report Dates:** 

# TABLE OF CONTENTS

# Volume 1 – November 4, 2016

			Page
1.0	INTE	RODUCTION	1
	1.1	Purpose of Study	1
	1.2	Authority and Acknowledgements	2
	1.3	Coordination	3
2.0	ARE	A STUDIED	4
	2.1	Scope of Study	4
	2.2	Community Description	4
	2.3	Principal Flood Problems	10
	2.4	Flood Protection Measures	15
3.0	ENG	INEERING METHODS	17
	3.1	Hydrologic Analyses	17
	3.2	Hydraulic Analyses	25
	3.3	Vertical Datum	29
4.0	FLO	ODPLAIN MANAGEMENT APPLICATIONS	31
	4.1	Floodplain Boundaries	31
	4.2	Floodways	32
		<u>Volume 2 – November 4, 2016</u>	
5.0	INSU	JRANCE APPLICATION	108
6.0	FLO	OD INSURANCE RATE MAP	109
7.0	OTH	ER STUDIES	110
8.0	LOC	ATION OF DATA	112
9.0	BIBI	LIOGRAPHY AND REFERENCES	113
10.0	REV	ISIONS DESCRIPTIONS	116
	10.1	First Revision	116

# <u>TABLE OF CONTENTS (Continued)</u> <u>Volume 1 – November 4, 2016</u>

# **FIGURES**

Figure 1 – Floodway Schematic

Table 7 - Revised Waterway Study Reaches

Exhibit 1 – Flood Profiles

33

118

# **TABLES**

Table 1 – Initial and Final CCO Meetings	3
Table 2 – Incorporated LOMRs	4
Table 3 – Summary of Discharges	19-24
Table 4 – Roughness Coefficient - Manning's "n" Values	27
Table 5 – Floodway Data	34-95
<u>Volume 2 – November 4, 2016</u>	
Table 5 – Floodway Data (Continued)	96-107
Table 6 – Community Map History	111

# **EXHIBITS**

Ash Creek	Panels	01P-02P
Beal Creek	Panel	03P
Beaverton Creek	Panels	04P-13P
Bethany Creek	Panel	14P
Bronson Creek	Panels	15P-19P
Butternut Creek	Panels	20P-24P
Cedar Creek	Panels	25P-26P
Cedar Mill Creek	Panels	27P-30P
Cedar Mill Creek – North Overflow	Panel	31P
Cedar Mill Creek – South Overflow	Panel	32P
Cedar Mill Creek – Upper North Overflow	Panel	33P
Celebrity Creek	Panel	34P
Chicken Creek	Panels	35P-36P
Chicken Creek – West Tributary	Panel	37P
Council Creek	Panels	38P-43P
Dairy Creek	Panels	44P-48P
Dawson Creek	Panels	49P-51P
Deer Creek	Panel	52P
Erickson Creek	Panels	53P-54P

# **TABLE OF CONTENTS (Continued)**

Fanno Creek Gales Creek Glencoe Swale Panels 55P-60P Panels 61P-65P Panels 66P-69P

# Volume 3 – November 4, 2016

Golf Creek	Panels 70P-71P
Gordon Creek	Panels 72P-73P
Hall Creek	Panels 74P-75P
Hall Creek – 106th Tributary	Panels 76P-77P
Hall Creek – North Fork	Panel 78P
Hall Creek – South Fork	Panel 79P
Hedges Creek	Panels 80P-81P
Holcomb Creek	Panels 82P-83P
McKay Creek	Panels 84P-86P
North Johnson Creek	Panels 87P-90P
North Johnson Creek – East Tributary	Panel 91P
North Johnson Creek – North Tributary	Panels 92P-94P
Nyberg Slough	Panels 95P-96P
Rock Creek North	Panels 97P-103P
Rock Creek South	Panels 104P-105P
South Johnson Creek	Panels 106P-107P
Storey Creek	Panels 108P-109P
Storey Creek – East Tributary	Panel 110P
Storey Creek – Middle Tributary	Panel 111P
Summer Creek	Panels 112P-113P
Tualatin River	Panels 114P-133P
Tualatin River - Golf Course Overflow	Panel 134P
Tualatin River - LaFolette Overflow	Panel 135P
Turner Creek	Panel 136P-137P
Unnamed Tributary of McKay Creek	Panels 138P-139P
Waible Creek	Panels 140P-142P
Waible Creek – South Tributary	Panel 143P
Waible Creek Tributary 1	Panel 144P
Waible Creek Tributary 2	Panel 145P
Wapato Creek	Panel 146P
West Fork Dairy Creek	Panel 147P
Willow Creek	Panels 148P-151P

# **PUBLISHED SEPARATELY**

Flood Insurance Rate Map Index

Flood Insurance Rate Map

# FLOOD INSURANCE STUDY WASHINGTON COUNTY, OREGON AND INCORPORATED AREAS

# 1.0 INTRODUCTION

# **1.1 Purpose of Study**

This Flood Insurance Study (FIS) revises and updates information on the existence and severity of flood hazards in the geographic area of Washington County, including the Cities of Banks, Beaverton, Cornelius, Durham, Forest Grove, Gaston, Hillsboro, King City, North Plains, Sherwood, Tigard, and Tualatin; and the unincorporated areas of Washington County (referred to collectively herein as Washington County), and aids in the administration of the National Flood Insurance Act of 1968 and the Flood Disaster Protection Act of 1973. This study has developed flood-risk data for various areas of the community that will be used to establish actuarial flood insurance rates and to assist the community in its efforts to promote sound floodplain management. Minimum floodplain management requirements for participation in the National Flood Insurance Program (NFIP) are set forth in the Code of Federal Regulations at 44 CFR, 60.3.

Please note that the Cities of Rivergrove, Tualatin, and Wilsonville are geographically located in Washington and Clackamas Counties. The City of Tualatin is included in its entirety in this FIS report. The flood-hazard information for the Cities of Rivergrove and Wilsonville are mapped entirely within Clackamas County. See the separately published FIS report and Flood Insurance Rate Map (FIRM) for Clackamas County, OR and Incorporated Areas.

Please note that the Cities of Lake Oswego and Portland are geographically located in Multnomah, Clackamas, and Washington Counties. The flood-hazard information for the City of Lake Oswego is mapped entirely within Clackamas County. The flood-hazard information for the City of Portland is mapped independently. See the separately published FIS reports and FIRMs for Clackamas County, OR and Incorporated Areas, and the City of Portland, OR.

In some States or communities, floodplain management criteria or regulations may exist that are more restrictive or comprehensive than the minimum Federal requirements. In such cases, the more restrictive criteria take precedence, and the State (or other jurisdictional agency) will be able to explain them.

## **1.2** Authority and Acknowledgments

The sources of authority for this FIS report are the National Flood Insurance Act of 1968 and the Flood Disaster Protection Act of 1973.

The hydrologic and hydraulic analyses for this study were performed by the U.S. Army Corps of Engineers (USACE), Portland District, for the Federal Emergency Management Agency (FEMA), under Inter-Agency Agreement Nos. H-7-76 and H-10-77. This work, which was completed in November 1980, covered all significant flooding sources affecting Washington County.

The Unincorporated study was revised on March 18, 1987, to incorporate existing conditions on overbank areas adjacent to Cedar Mill Creek between Southeast Murray Boulevard and Southwest Jenkins Road (Cross Sections H and J). The width of the floodway for this reach was narrowed by 64 feet at Cross Section H and by 6 feet at Cross Section I. In addition, the corporate limits of the county were revised on the FIRMs and Flood Boundary and Floodway Map (FBFMs) to indicate areas annexed by the City of Beaverton. These annexations placed a reach of Willow Creek just south of Interstate Highway 26 within the City of Beaverton.

The final coordination meeting for the original study for the Tualatin River was held on February 1, 1981, and was attended by representatives of FEMA, the Study Contractor, and the Washington County Departments of Public Works and Planning. No requests for changes were made at that time. A coordination meeting, attended by representatives of the USACE, Portland District, and FEMA, was held on July 20, 1984. This meeting resulted in the reanalysis of the Tualatin River and Nyberg Slough.

In 2005 a restudy was done to incorporate new floodplain data for Ash Creek, Fanno Creek, and Summer Creek, and to incorporate the channel improvement project within the reach of the Tualatin River. The hydrologic and hydraulic analyses for the Ash Creek, Fanno Creek, and Summer Creek restudy were performed by Pacific Water Resources Inc., for Clean Water Services (formerly Unified Sewerage Agency) of Washington County and submitted to FEMA under the Cooperating Technical Partners program. This restudy was completed on June 30, 2000. This revision was requested by Washington County because of the effects of the largest flood since 1980, which occurred along Fanno Creek in February 1996. The February 1996 flood had an estimated recurrence interval of approximately 25 years.

# 1.3 Coordination

Consultation Coordination Officer's (CCO) meetings may be held for each jurisdiction in this countywide FIS. An initial CCO meeting is held typically with representatives of FEMA, the community, the state, and the study contractor to explain the nature and purpose of a FIS and to identify the streams to be studied by detailed methods. A final CCO meeting is held typically with representatives of FEMA, the community, and the study contractor to review the results of the study. All problems raised at these meetings have been addressed in this study.

The dates of the initial and final CCO meetings held for Washington County and the incorporated communities within its boundaries are shown in Table 1, "Initial and Final CCO Meetings."

Community	Initial CCO Date	Final CCO Date
Beaverton, City of	September 10, 1976	October 29, 1982
Cornelius, City of	September 8, 1976	January 29, 1981
Durham, City of	September 10, 1976	April 18, 1980
Forest Grove, City of	September 9, 1976	April 10, 1981
Gaston, City of	September 9, 1976	July 21, 1981
Hillsboro, City of	September 8, 1976	September 12, 1980
King City, City of	September 9, 1976	February 1, 1981
North Plains, City of	October 22, 1976	April 10, 1981
Portland, City of	September 25, 1974	April 30, 1980
Rivergrove, City of	June 1977	August 21, 1986
Sherwood, City of	September 10, 1976	January 29, 1981
Tigard, City of	September 9, 1976	April 9, 1981
Tualatin, City of	September 9, 1976	February 1, 1981

**Table 1. Initial and Final CCO Meetings** 

The results of this revised study were reviewed at two final CCO meetings. The first CCO meeting was held on November 6, 2007, and attended by representatives of Washington County and the cities of Banks, Cornelius, Forest Grove, Hillsboro, North Plains, and by FEMA's Region X representatives. The second meeting was held on November 7, 2007 and attended by representatives of Washington County and the cities of Beaverton, Durham, Sherwood, and Tualatin, and by FEMA's Region X representatives. All problems raised at that meeting have been addressed in this study.

# 2.0 AREA STUDIED

# 2.1 Scope of Study

This FIS report covers the geographic area of Washington County, Oregon, including the incorporated communities listed in Section 1.1. The areas studied by detailed methods were selected with priority given to all known flood hazards and areas of projected development.

Approximate analyses were used to study those areas having a low development potential or minimal flood hazards. The scope and methods of study were proposed to, and agreed upon, by FEMA and the communities.

This initial countywide FIS (November 4, 2016) incorporated the determination letters issued by FEMA resulting in map changes (Letters of Map Change, or LOMCs). All Letters of Map Revision (LOMRs) incorporated into this FIS are summarized in Table 2. The Letter of Map Change (LOMC) actions for previously-issued LOMCs for Washington County are summarized in the Summary of Map Amendment (SOMA) included in the Technical Support Data Notebook (TSDN) associated with this FIS update. Copies of the TSDN may be obtained from the Community Map Repository.

Community	LOMC Case No	Flooding Source(s)	Date Issued	LOMC Type
Beaverton, City of	06-10-B213P	Fanno Creek	11/6/2006	LOMR
Tigard, City of	07-10-0375A	Redrock Creek	4/10/2007	LOMR-F
Hillsboro, City of	14-10-1241P	Waible Creek – South Tributary	8/15/2014	LOMR
Hillsboro, City of Washington County, Unincorporated Areas	14-10-1501P	Waible Creek, Waible Creek Tributary 1, Waible Creek Tributary 2	12/29/2014	LOMR

# Table 2. Incorporated LOMRs

# 2.2 Community Description

Washington County is located in northwestern Oregon. It is bordered on the north by Columbia County, on the south by Yamhill and Clackamas Counties, on the west by Tillamook County, and on the east by Multnomah and Clackamas Counties. Because of its location adjacent to the City of Portland, Washington County experienced rapid growth during the mid-20th century; the population increased from 39,194 in 1940 to 215,000 in 1978 (Reference 1). Most of that increase occurred in the southeastern part of the county. The estimated population in 2010 was 529,710 (Reference 2).

All of the streams considered in this study are part of the Tualatin River drainage basin. The Tualatin River originates in the Coast Range at an elevation of 3,400 feet. The basin has an area of 711 square miles (sq. mi.) and is oval; it is approximately 40 miles long and 25 miles wide. The Tualatin River basin is located in central Washington County. The major portion of the Tualatin River floodplain is widest in the stream length located 7 miles upstream of the mouth to 70 miles upstream of the mouth.

The climate in Washington County is characterized by cool, wet winters and warm, dry summers. Maritime influences mostly dominate the area throughout the year. The average temperature in January is 38°F, and in July the average temperature rises to 66.5°F.

The average annual precipitation for the county is 38.0 inches, which primarily occurs during the months of October through March. Snowfall occurs only a few days each year. Snow on the ground does not last long, and depths seldom exceed 6 inches (Reference 1).

The Tualatin River valley is a broad synclinal valley, and the area of the valley floor represents a large percentage of the total watershed. The upland areas are underlain with basaltic lavas and volcanics, shale, sandstone, and conglomerates, all of which are deeply weathered and covered with loam and clay loam soils capable of supporting dense growths of vegetation. Exceptionally heavy and extended periods of rainfall cause excessive runoff and severe erosion, especially in cleared and burned areas. Two soil groups, the older valley filling and the recent alluvial soil, are represented on the valley floor where drainage, both on the surface and internal, varies from good to poor. Poor drainage at the lower end of the valley can be attributed, in part, to the existence of reefs or ledges of basaltic rock, which have established a temporary base level for the valley (Reference 3).

The uplands of the basin are generally covered with heavy fir timber that has a thick undergrowth and a mat of ferns. Extensive timber cutting has taken place in this part of the basin; however, after a few years, the previous undergrowth reestablishes itself and is supplemented by ferns and wild blackberry vines. Further down the slopes, the timber thins out on the valley floor until it is limited to small, scattered areas. Within the floodplain, scattered scrub oak trees with bands of willow, alder, and brush, as many as several hundred yards in width, parallel both banks of all major watercourses (Reference 3).

## City of Beaverton

The City of Beaverton is on the eastern edge of Washington County. It is approximately 11 miles southwest of Portland, Oregon. The city, which was incorporated in 1893, grew to an estimated population of 89,803 in 2010 (Reference 2). Beaverton is bordered by the City of Tigard on the south and by the unincorporated areas of Washington County on all other sides.

Beaverton is a fast-growing community, with a diversified economic base centered around numerous offices and several light industries, including electronics and food processing. In addition, its proximity to Portland gives it many characteristics of a bedroom community. Commercial development is centered in the northern portion of Beaverton, specifically along Cedar Hills Boulevard, Tualatin-Valley Highway, Canyon Road, and Beaverton-Hillsdale Highway.

# City of Cornelius

The City of Cornelius is located in central Washington County. It is situated approximately 15 miles west of Portland. Cornelius was incorporated in 1893 and has grown from a population of 3,450 in 1978 to an estimated 11,869 in 2010 (References 4 and 2, respectively).

Very little development has taken place within the flood plains of Cornelius. The majority of development is south of Council Creek in eastcentral Cornelius. Commercial and industrial properties are primarily along major transportation routes. These routes include Tualatin Valley Highway, Burlington Northern Railroad, and Southern Pacific Railroad.

#### City of Durham

The City of Durham is located in the southeastern corner of Washington County. It is approximately 5 miles southwest of the City of Portland, Oregon. The city had an estimated population of 1,351 in 2010 (Reference 2).

The Tualatin River originates in the Coast Range at an elevation of 3,400 feet. The watershed has an area of 711 sq. mi., is oval in shape, and is approximately 40 miles long and 25 miles wide. The topography abruptly changes to a very flat valley and a wide floodplain in the area where Tualatin River emerges from the foothills. The river flows southeasterly through Durham, forming a portion of the southern corporate limits of the city.

Economic activity for this small community is diversified and characterized by non-retail commercial and light industrial uses. For

example, the headquarters for a building contractor and a distribution/trucking depot are located in Durham. In addition, several businesses and office park developments have been constructed on the east side of the Southwest Upper Boones Ferry Road, which serves as the principal transportation corridor through the city. Residential development is characterized by low density single family housing located primarily west of the Southwest Upper Boones Ferry Road. A high density 210 unit apartment development is located in southeast Durham. Floodplains are virtually undeveloped and are planned to remain as permanent open space for park and recreation purposes.

## City of Forest Grove

Forest Grove is in central Washington County. It is approximately 21 miles west of Portland, Oregon. The city was incorporated in 1872 and has grown to a population of 21,083 in 2010 (Reference 2).

Forest Grove has a stable economic base, revolving around food processing and wood-products industries. Commercial development is primarily along Tualatin Valley Highway. Due to its proximity to Portland, Forest Grove has also developed into a suburban community. The flood plains are relatively undeveloped. Considerable open space for future development exists outside of the flood plains of Tualatin River, Gales Creek, and Council Creek.

#### City of Gaston

Gaston is located on the southern border of Washington County. It is approximately 29 miles west of Portland, Oregon. The City of Gaston was incorporated in 1914. The population in 2010 was estimated to be 637 (Reference 2). It is bordered by unincorporated Washington County land to the north, east, and west, and by unincorporated Yamhill County land to the south.

Economic activity in Gaston is centered around forestry and agricultural industries, with food processing playing an especially key role. Commercial development is located primarily along the Tualatin Valley Highway/South Pacific Railroad corridor through the town. Residential development is generally limited to the western portion of Gaston. Only the eastern edge of Gaston is considered flood prone. Several residences in that portion of the community are in the Tualatin River flood plain.

#### City of Hillsboro

Hillsboro is in central Washington County. The city is approximately 17 miles west of Portland, Oregon. Hillsboro was incorporated in 1876 and had a population of 91,611 in 2010 (Reference 2).

Hillsboro has a rapidly expanding and diversified economy centered around numerous light manufacturing plants. In particular, the electronics industry is becoming more important in the economy of Hillsboro. Due to its proximity to Portland, Hillsboro also has characteristics of a bedroom, or suburban, community. Commercial development in Hillsboro is extensive, with a well-developed business district in the west-central portion of the city and heavy commercial development along Tualatin Valley Highway. Residential areas are scattered throughout the city but are concentrated in the northern and eastern portions of Hillsboro. Important transportation routes in the city include Tualatin Valley Highway (State Highway 8), Sunset Highway (U.S. 26), Cornell Road, State Highway 219, Burlington Northern Railroad, and Southern Pacific Railroad. The flood plains are relatively undeveloped.

#### City of King City

The City of King City is located in the North Willamette Valley in Washington County. The nearest major highway is Interstate 5 and the nearest major city is Tigard. King City was incorporated in 1966 and had a population of 3,111 in 2010 (Reference 2).

#### City of North Plains

North Plains is located in north-central Washington County. It is approximately 20 miles west of Portland, Oregon. The city was incorporated in 1963 and had a population of 1,947 in 2010 (Reference 2).

The economy of North Plains is based primarily on agriculture and forestry. Soil types in the city consist of the Woodburn, Aloha, and Willamette Associations. Vegetation consists of grass, Douglas fir, oak, ash, willow, cedar, hazelbrush, maple, and rosebushes. The floodplains in the community are generally undeveloped.

# City of Sherwood

Sherwood is located in the southeast corner of Washington County. It is approximately 13 miles southwest of Portland, Oregon. The population in 2010 was 18,194 (Reference 2).

Economic activity in Sherwood is diversified and growing. Industrial facilities in the community include a wood products plant, a leather tannery, and a machine manufacturing plant. In addition, agriculture and support services augment the income of the community. Commercial development is primarily in the central section of Sherwood. Residential development is spread throughout the city. Important transportation routes are Pacific Highway West (State Highway 99), Edy Road, Sherwood

Road, and the Southern Pacific Railroad. There is no development in the flood plain.

# City of Tigard

Tigard is in the southeast corner of Washington County. It is approximately 8 miles southwest of Portland, Oregon, and is adjacent to the City of Beaverton to the north and to the City of Durham to the south. Unincorporated areas of Washington County also border Tigard, along with some small county areas that are within the city. Tigard was incorporated in 1961; the estimated population in 2010 was 48,035 (Reference 2).

Economic activity in Tigard is diversified and growing. Industrial facilities in the community are varied and are located along Pacific Highway West (State Highway 99W) and State Highway 217 (US217). Commercial development is located primarily along Pacific Highway West and Southwest Main Street. Residential development in Tigard is mostly west of Fanno Creek. Important transportation routes in the city are Pacific Highway West, US217, Hall Boulevard, and the Burlington Northern and Southern Pacific Railroads. The floodplains of several areas along the studied stream reaches are undergoing development. One such area is along Summer Creek between Southwest 113<sup>th</sup> and Southwest 121<sup>st</sup> Avenues, where several residences are in the floodplain. Another floodprone area includes commercial and residential development along a 1-mile reach of Fanno Creek from Pacific Highway West upstream to Southwest Tiedeman Avenue.

# City of Tualatin

Tualatin is in the southeastern corner of Washington County and the northwestern portion of Clackamas County. It is bordered by the City of Durham, to the north, by the City of Lake Oswego to the east, and by unincorporated areas of Washington and Clackamas Counties to the west and south. Tualatin is approximately 5 miles southwest of the City of Portland. The population was estimated to be 26,054 in 2010 (Reference 2).

The broad-based economy of Tualatin is subject to strong growth. Most of the economic activity centers in the central business district, where commercial development is interspersed with local industries. In the central business district, development includes new large retail chain stores. Industrial development in this area includes a food-processing plant and several warehouses. Residential development is concentrated in the northwestern and southwestern portions of Tualatin. New development is occurring throughout the southern portion of Tualatin on the benchlands above the Nyberg Slough flood plain.

# 2.3 Principal Flood Problems

The past history of flooding of the streams within Washington County indicates that, for a particular storm, flooding usually occurs on many streams throughout the study area. Flooding is caused by heavy rainfall augmented by snowmelt at a time when the soil is near saturation. Damaging floods may occur any time between late October and late April. The most severe floods occur in December, January, and February.

The largest flood recorded on the Tualatin River at West Linn since the U.S. Geological Survey (USGS) established a stream gage there in 1928 occurred in December 1933. The peak discharge at the gage was 23,300 cubic feet per second (cfs) with a 1.4-percent-annual-chance of flooding. The January 1974 flood on the Tualatin River also caused considerable damage to the study area. That flood had an estimated discharge of 22,300 cfs with a 4-percent-annual-chance of flooding. The flood occurred before the operation of the Henry Hagg Lake Project (Reference 6). The operation of the Henry Hagg Lake Project has decreased the frequency of a flood of 21,500 cfs to a 2-percent-annual-chance of flooding for the Tualatin River at West Linn.

Other major Tualatin River flood occurred in December 1937, December 1955, December 1964, January 1974, and February 1996. Before 1928, flooding was not well documented, but major floods occurred in February 1890, November 1896, February 1904, January 1905, and January 1914.

The February 1996 flood on the Tualatin River was the largest flood flow ever recorded with an estimated 84-year return interval and an annual probability of recurrence of 1.2%. However, for almost all of the smaller urbanized Tualatin River tributaries that were studied, the November 1996 flood is thought to be the largest flood ever observed with an estimated 25-year return interval and an annual probability of recurrence of 4%.

Records of past flood on the remaining study reaches in Washington County are not well documented. Flood damages have been small in these unincorporated areas because their floodplains are sparsely developed.

However, the floodplain of Nyberg Slough is not sparsely developed. In the 1974 flood, a business district sustained heavy damage when the Tualatin River overtopped its banks and entered Nyberg Slough, an overflow channel. A Tualatin River flood with a recurrence interval greater than 15 years would be expected to flow through Nyberg Slough.

## City of Beaverton

No gaging stations are located along Beaverton Creek, Fanno Creek, South Johnson Creek, Erickson Creek, or Cedar Mill Creek. However, history indicates that Beaverton has had recurrent and substantial flood problems from these streams. The largest flood along the creeks in the study area since 1970 occurred in December 1977. The 1977 flood had an estimated recurrence interval of approximately 10 years. Flood damage in Beaverton was moderate; most occurred near the intersections of SH 217 with SH 8 and SH 10.

The potential for property damage from Beaverton Creek overflows is especially severe for several reasons. The inadequate size and moderate grade of the channel through the study segment causes overbank flooding during even mild storms. Beaverton Creek flow is constricted by many culverts and bridges, resulting in increased upstream flood heights. Finally, the potential for property damage is significant because of the extensive commercial and residential development within the Beaverton Creek floodplain.

Fanno Creek, South Johnson Creek, Erickson Creek, and Cedar Mill Creek also have flooding problems. However, the flood damage potential from these streams is not as large as that from Beaverton Creek. Generally, the floodplains along these streams have not been extensively developed. The only area with a major flooding problem is a residential development in the Fanno Creek floodplain just upstream of SH 217.

# City of Cornelius

Since October 1939, the USGS has maintained a stream gage on Tualatin River near Dilley, Oregon. The largest flood at that gage occurred in December 1964, when a flow of 17,100 cfs was observed. The average return interval for the 1964 flood was 190 years. Major floods were also recorded at Dilley in December 1955, January 1964, January 1972, and January 1974. All peak discharges after 1974 were affected by regulation or diversion, and are thus not considered major floods. Prior to 1939, flooding was not well documented in the upper Tualatin River basin. However, records from a gage on Tualatin River near West Linn, Oregon, indicate major floods occurred in December 1933 and December 1937.

Generally, Cornelius is free of flood damage by riverine sources because there is almost no development in the flood plain.

#### City of Durham

Five major floods have occurred on the Tualatin River at Durham since the USGS established a stream gage at West Linn in 1928. Those floods occurred in December 1933, December 1937, December 1955, December 1964, and January 1974, and had return intervals of approximately 90, 45, 20, 10, and 25 years, respectively. These floods had peak discharges of 28,300; 25,300; 21,400; 17,700; and 22,000 cfs, respectively, at the West Linn gage. All peak discharges after 1974 were affected by regulation or diversion, and are thus not considered major floods. Considerable development in Durham took place on high ground, resulting in only minor flood damage to property.

Fanno Creek has flooded low areas downstream of Durham Road. However, damage has been slight because of minimal development in the floodplain. Fanno Creek has no major obstructions that aggravate flooding problems in Durham.

#### City of Forest Grove

The USGS has maintained two stream gages on Gales Creek periodically since 1935; one near the Town of Gales Creek, period of record 1936 to 1945 and 1964 to 1970, and the other near Forest Grove, period of record 1941 to 1956 and 1971 to 1980. The largest recorded flood at either station occurred in February 1949 when a discharge of 6410 cfs, a 5.9-percent-annual-chance flood, was recorded near Forest Grove. Other major floods have been recorded in December 1955, January 1964, December 1964, January 1972, and December 1977. There are no stream gages on Council Creek.

Due to the undeveloped or lightly developed state of the flood plains within Forest Grove, damages caused by flooding have been minimal. Water-related damage in the city generally results from high ground water and local drainage problems.

#### City of Gaston

The largest recorded flood on Tualatin River in the vicinity of the City of Gaston occurred in December 1964. The peak discharge at the USGS stream gage near Dilley, 4 miles downstream of City of Gaston, was 17,100 cfs. The 1964 flood was a 0.5-percent-annual-chance flood. That flood caused minor damage to residences located east of Tualatin Valley Highway in Gaston. There have been numerous other large floods on Tualatin River, including those which occurred in 1933, 1937, 1955, 1972, and 1974.

The largest flood on Wapato Creek occurred in 1949. Although stream gage records are not available, it is estimated that the 1949 flood was a 2-percent-annual-chance flood. Flood damages in Gaston were light because development in the flood plain had been avoided.

# City of Hillsboro

The City of Hillsboro is generally free of flood damage from riverine sources. Most damage in the city results from higher ground water and ineffective local drainage.

## City of King City

Intense rainfall runoff from massive winter storms moving inland from the Pacific Ocean has combined with snowmelt runoff to produce large Tualatin River floods. The largest flood recorded at the City of West Linn since the USGS established a stream gage there in 1928 occurred in December 1933. The peak discharge at the gage was 23,300 cfs, with an approximate recurrence interval of a 1-percent-annual-chance flood.

The city of King City is affected by the Tualatin River but damage is small because of the limited development in the flood plain. Past damages in the city resulted from high ground water and ineffective local drainage.

## City of North Plains

Flooding in North Plains is caused by intense rainfall from massive winter storms moving inland from the Pacific Ocean. This often results in simultaneous flooding on all streams in the study area, as in the flood of December 1964. Flooding on the unnamed tributary downstream of Glencoe Road at River Mile (RM) 0.27 is greatly accentuated by coincident flooding on McKay Creek. Flooding upstream of Glencoe Road is also influenced by the backwater effect of McKay Creek. The 1.8-mile study reach has several highly constrictive culverts that cause substantial ponding. This includes the culvert crossing at Glencoe Road (RM 0.27) and the Burlington Northern Railroad (BNRR) culvert crossing at RM 1.20. At the BNRR culvert crossing, backwater from the 10-percent-annaul-chance flood and greater floodflows would overflow the right bank at Gordon Road.

There are no stream gage stations on either McKay Creek or Unnamed Tributary of McKay Creek, but local officials and residents have substantial knowledge of flooding conditions through the study reach. Local officials indicate that floods rise quickly following a rainstorm and may last a full day. Coincident flooding on McKay Creek is primarily responsible for this relatively long flood duration for a small stream of 2.5 square miles drainage area. The constrictive culverts at RM 0.27 and RM 1.20 also contribute to the extended duration.

The most recent flood on January 31, 1987, closely followed this pattern of flood duration and coincident flooding on McKay Creek. Based on numerous high water marks, flood photographs, and interviews with local

officials and residents, the January 31, 1987, flood was estimated to be greater than a 10-year recurrence interval. Flood damages were minor, however, consisting of numerous closed roads and isolation for several property owners. Flooding has occurred on a fairly regular basis on the Unnamed Tributary, and that knowledge has discouraged development in the floodplain.

#### City of Sherwood

Flooding from Cedar Creek and Rock Creek South is generally caused by rainfall in the winter, the period of greatest storm activity. Flood rise quickly following a heavy rainstorm and usually last less than 1 day.

The largest flood on both streams in the last 30 years occurred in December 1977. Heavy rains at that time caused some shallow flooding along the Rock Creek South flood plain. Sherwood Road, the main arterial to the City of Tualatin, was under approximately 1 foot of floodwater from Rock Creek South. No structures located along Rock Creek South were reported flooded. Flood damage from Cedar Creek was negligible because that stream is in a ravine.

## City of Tigard

Flooding on the Tualatin River, Fanno Creek, Ash Creek, and Summer Creek is primarily caused by rainstorms in the winter, the period of greatest storm activity. Floods rise quickly following a heavy rainstorm and usually last less than 1 day on Fanno Creek and half a day on Ash and Summer Creeks.

Flooding in Tigard is not well documented. During the last 30 years, the largest flood on Fanno, Ash, and Summer Creeks occurred in December 1977. Although stream gage records are not available, it is estimated that the 1977 flood recurrence interval was approximately a 10-percent-annual-chance flood for the three streams. Flood damages in Tigard were minor because the areas susceptible to flooding were known and development was avoided in those areas. Flooding along Summer Creek is accentuated by a high ground water table, which causes nuisance flooding that affects numerous residences.

#### City of Tualatin

Intense rainfall runoff from massive winter storms moving inland from the Pacific Ocean has combined with snowmelt runoff to produce large Tualatin River floods. The largest flood recorded at the City of West Linn since the USGS established a stream gage there in 1928 occurred in December 1933. The peak discharge at the gage was 23,300 cfs, with an approximate recurrence interval of a 1-percent-annual-chance flood. The

central business district of Tualatin sustained heavy damage when the Tualatin River overtopped its banks and entered Nyberg Slough. A Tualatin River flood with greater than a 6.6-percent-annual-chance flood would be expected to flow through Nyberg Slough and inundate much of the central business district.

The January 1974 flood on the Tualatin River caused considerable damage to the study area. That flood had an estimated discharge at Tualatin of 22,340 cfs, which was estimated to be a 2.5-percent-annual-chance flood. The central business district, located on Nyberg Slough, was hit especially hard. Peak Nyberg Slough flow was approximately 2,600 cfs.

Flooding on Hedges Creek is often elevated by Tualatin River backwater flooding. Urbanization of the Hedges Creek drainage basin could increase future flood problems.

# 2.4 Flood Protection Measures

The Tualatin River basin has one multipurpose flood-control storage project. The Henry Hagg Lake Project, located northwest of the City of Gaston, was constructed by the U.S. Bureau of Reclamation (USBR). That project began operation in the 1974-75 flood season. It provides 30,000 acre-feet of flood storage starting in November of each year. Flood storage capacity is reduced as the winter flood season terminates, and the reservoir is filled each spring in anticipation of the summer irrigation demand. This storage would reduce the discharge of a flood, such as the flood of 1964, by approximately 3,000 cfs. The effect of Henry Hagg Lake Project flood storage has been considered in the calculation of water-surface profiles for the Tualatin River reach in the following communities: Cornelius, Durham, Forest Grove, Gaston, Hillsboro, King City, Tigard, and Tualatin.

The USBR has completed a draft feasibility study of two alternative storage project on the Tualatin River near Gaston, which could provide additional flood storage in the Tualatin River Basin. Those projects, however, are still in the planning stages and are not reflected in the data presented (Reference 6).

Nonstructural measures are also being used to aid in the prevention of future flood damage. These measures are based on a flood hazard zoning ordinance for controlling development within the 1-percent-annual-chance floodplain. This ordinance requires the county or the city to review all proposed development within the 1-percent-annual-chance floodplain to ensure that it is reasonably safe from flooding. The FEMA guidelines for controlling development within the flood plain are followed (Reference 7).

#### City of Beaverton

No structural flood protection measures are being used to help prevent future flood damage in Beaverton, but several culverts have been enlarged on Beaverton Creek to improve the flooding situation. The Southern Pacific Railroad culvert was improved, as were numerous culverts in the Canyon Road area.

## City of Gaston

There is a levee along the right bank of Wapato Creek which was considered in the analysis of flood elevations. However, the levee does not provide 1-percent-annual-chance flood protection.

# 3.0 ENGINEERING METHODS

For the flooding sources studied by detailed methods in the community, standard hydrologic and hydraulic study methods were used to determine the flood-hazard data required for this study. Flood events of a magnitude that is expected to be equaled or exceeded once on the average during any 10-, 50- 100-, or 500-year period (recurrence interval) have been selected as having special significance for floodplain management and for flood insurance rates. These events, commonly termed the 10-, 50-, 100-, and 500-year floods, have a 10-, 2-, 1-, and 0.2-percent chance, respectively, of being equaled or exceeded during any year. Although the recurrence interval represents the long-term, average period between floods of a specific magnitude, rare floods could occur at short intervals or even within the same year. The risk of experiencing a rare flood increases when periods greater than 1 year are considered. For example, the risk of having a flood that equals or exceeds the 1-percent-annual-chance flood in any 50-year period is approximately 40 percent (4 in 10); for any 90-year period, the risk increases to approximately 60 percent (6 in 10). The analyses reported herein reflect flooding potentials based on conditions existing in the community at the time of completion of this study. Maps and flood elevations will be amended periodically to reflect future changes.

# 3.1 Hydrologic Analyses

Hydrologic analyses were carried out to establish peak dischargefrequency relationships for each flooding source studied by detailed methods affecting the community. Some of the flooding sources in the discussion below are superseded with new studies. Pease refer to section 10 for details of updates.

Tualatin River stream-gage records were analyzed statistically, using the log-Pearson Type III distribution, as outlined by the U.S. Water Resources Council (Reference 8). Discharge-frequency curves for USGS stream gages at West Linn, Dilley, and Farmington were developed utilizing records from 1938 to 1976, 1940 to 1975, and 1939 to 1958, respectively.

As a result of the relatively short record, Farmington gage data were adjusted using the long-term station data at West Linn. All downstream discharges were adjusted for flood control furnished by the Henry Hagg Lake Project.

Peak Tualatin River discharges near the downstream corporate limits of Tualatin were reduced to reflect flows into Oswego Canal by way of a diversion dam and outlet works. The Oregon Iron and Steel Dam at RM 3.4 and its outlet work at RM 6.7 divert flow from the Tualatin River into Oswego Canal to stabilize the Lake Oswego water level. A stream gage on

Oswego Canal has been maintained by the USGS since 1928 to measure this outflow from the Tualatin River.

The USGS has maintained two stream gages on Gales Creek periodically since 1935; one near the Town of Gales Creek, with periods of record from 1936 to 1945 and from 1964 to 1970, and the other near the City of Forest Grove, with periods or record from 1941 to 1956 and from 1971 to the present. The U.S. Water Resources Council guidelines (Reference 8) for broken record stations were applied to these sets of data, and discharge-frequency curves were prepared for both stations.

Peak discharge-drainage are relationships for selected recurrence intervals on Dairy Creek, West Fork Dairy Creek, McKay Creek, and Unnamed Tributary of McKay Creek were obtained from a Myer's rating curve developed from several nearby stream gages. These gages included three on the Tualatin River, one on Gales Creek, and one on Johnson Creek in Multnomah County, respectively.

The frequency discharges for the Unnamed Tributary of McKay Creek were developed by the regional analysis presented in "Magnitude and Frequency of Floods in Western Oregon," U.S. Geological Survey Open-File Report 79-553, dated 1979 (Reference 9). The frequency discharges developed by this procedure were checked for reasonableness of results.

The U.S. Natural Resources Conservation Service, formerly the Soil Conservation Service (SCS), method for rainfall-runoff and unit hydrograph determination (Reference 10) was used in conjunction with USACE computer programs (Reference 11, 12, and 13) for hydrograph computing, combining, and routing, for the purpose of generating flood hydrographs for selected recurrence intervals on the remaining detailed study streams in Washington County.

Peak flows from the July 1981 FIS report for the City of Durham (Reference 15) were used for the Fanno Creek restudy. The discharges used for the Tualatin River are taken from the channel improvement restudy of the Tualatin River, completed in 1983 by the USACE, as shown in the February 1987 FIS report for the City of Tualatin.

Peak discharge-drainage area relationships for Washington County are shown in Table 3, Summary of Discharges.

	Peak Discharges (cubic feet per second)				
	Drainage Area	10-Percent-	2-Percent-	1-Percent-	0.2-Percent-
Flooding Source and Location	(square miles)	Annual-Chance	Annual-Chance	Annual-Chance	Annual-Chance
Ash Creek					
At mouth	4.0	750	950	1,000	1,250
At Hall Boulevard	2.5	450	600	650	800
Beaverton Creek					
Upstream of Bronson Creek Confluence	31.4	3,943	5,063	5,518	6,605
At Cedar Hills Boulevard	6.5	1,039	1,353	1,480	1,771
Bronson Creek					
At mouth	5.0	518	656	714	855
At Northwest Kaiser Road	3.2	351	443	482	577
Butternut Creek					
At mouth	5.0	682	865	941	1,116
At Southwest 198th Avenue	2.9	498	628	680	801
At Southwest 185th Avenue	1.8	302	380	412	484
Cedar Creek					
At mouth	89	744	863	909	1.028
At State Highway 99 W	83	753	851	897	1,020
At Sunset Blvd	6.5	844	1 208	1 359	1,010
At Sunset Diva	0.0	044	1,200	1,559	1,752
Cedar Mill Creek					
At mouth	8.4	1,050	1,289	1,384	1,588
At Northwest Barnes	3.0	467	585	632	699
Cedar Mill Creek - North overflow	3.4	65	181	230	306
Cedar Mill Creek - South Overflow					
At mouth	3.5	9	84	120	180
Cedar Mill Creek - Upper North Overflow	3.4	57	141	164	198
Calabrity Graat					
At mouth	0.8	150	100	202	228
At mouning US of Pose park pedestrian bridge	0.8	130	100	205	238 200
US of Rosa park pedestrian ondge	0.7	127	130	1/1	200

	Peak Discharges (cubic feet per second)				
Flooding Source and Location	Drainage Area (square miles)	10-Percent- Annual-Chance	2-Percent- Annual-Chance	1-Percent- Annual-Chance	0.2-Percent- Annual-Chance
Chicken Creek					
At mouth	15.6	1125	1429	1580	1959
US of Cedar Creek confluence	8.9	744	863	909	1028
At Wilsonville road	6.5	939	1,321	1,502	1889
Chicken Creek - West Tributary					
At mouth	1.6	309	425	477	611
Council Creek					
At Hobbs Road	10.8	1,089	1,819	1,952	2,264
At Cornelius Schefflin Road	7.2	875	1,408	1,502	1,722
At Martin Road	5.0	609	1,005	1,077	1,245
At Beal Road	206.0	240	407	438	514
Dairy Creek					
Downstream of McKay Creek Confluence	296.4	19,513	30,176	32,847	37,816
Downstream of McKay Creek Confluence	230.2	15,104	23,793	25,396	29,247
Dawson Creek					
At mouth	4.3	601	755	819	976
At N.W. Brookwood Avenue	3.7	517	652	706	836
Erickson Creek					
At mouth	1.7	278	352	382	451
Farmington road	1.5	99	162	188	249
SW 9th Ave	0.7	115	146	158	186
Fanno Creek					
At mouth	32.0	2,950	3,850	4,250	5,150
At Southwest Tiedeman Avenue	24.0	2,750	3,500	3,850	4,700
At Southwest Dakota Street	17.0	1,900	2,450	2,700	3,250
At State Highway 217	10.0	1,400	1,800	1,970	2,400
At Washington-Clackamas County boundary	5.0	950	1,150	1,300	1,550

		Peak Discharges (cubic feet per second)				
Flooding Source and Location	Drainage Area (square miles)	10-Percent- Annual-Chance	2-Percent- Annual-Chance	1-Percent- Annual-Chance	0.2-Percent- Annual-Chance	
Gales Creek	; •					
At Stringtown Road	69.0	6,000	8,400	9,450	12,000	
At Roderick Road Gage	66.0	5,800	8,150	9,150	11,600	
Glencoe Swale						
At mouth	3.78	266	337	349	368	
Shannon road	2.6	346	599	645	753	
Jackson school road	2.3	321	552	594	692	
15th Avenue	1.9	247	432	464	543	
Sewell Avenue	0.8	98	171	185	217	
Golf Creek						
At mouth	1.4	317	389	419	488	
Gordon Creek						
At mouth	1.5	157	191	205	236	
Hall Creek						
At mouth	4	720	923	1001	1179	
Hwy 217 & 114th Ave	2.9	540	686	741	872	
Kennedy St	2.4	490	611	660	774	
Near 99th Ave	1	182	229	249	294	
Hall Creek - 106th Tributary						
At mouth	0.2	50	63	68	80	
Hall Creek - North Fork						
At mouth	1.0	189	239	259	306	
Hall Creek - South Fork						
At mouth	0.3	22	38	46	62	
Hedges Creek						
At mouth	4.1	304	509	595	802	
Upstream end	2.0	447	583	636	760	

#### Peak Discharges (cubic feet per second) 10-Percent-**Drainage Area** 2-Percent-1-Percent-0.2-Percent-Flooding Source and Location (square miles) **Annual-Chance** Annual-Chance Annual-Chance Annual-Chance Holcomb Creek 4.9 370 477 524 634 At mouth McKay Creek At mouth 66.0 4,409 6,983 7,451 8,569 At Hornecker Road 61.0 4,168 6,681 7,136 8,236 At West Union 38.7 2,811 4,328 4,603 5,271 North Johnson Creek 501 At mouth 3.5 425 530 598 North Johnson Creek - East Tributary 0.3 42 52 57 67 At mouth North Johnson Creek - North Tributary At mouth 0.5 94 118 127 150 Nyberg Slough At Southwest 65th Street 694.0 16,000 23,900 33,600 48,500 Rock Creek North At mouth1 76.0 6,765 8,682 9,492 11,432 Downstream of Dawson Creek confluence 70.0 6,412 8,213 8,971 10,779 At S.W. 231st Avenue (Below Beaverton Creek Confluence) 63.8 5,995 7,680 8,387 10,076 Upstream of Beaverton Creek confluence 26.0 1,872 2,411 3,210 2,640 At West Union Road 19.0 1,470 1,904 2,530 2,085 Rock Creek South 873 At mouth 6.2 520 660 718 At Sherwood Road 3.7 410 546 616 786 South Johnson Creek 730 793 940 At mouth 3.6 577 Storey Creek At mouth 5.0 396 657 706 828

		Peak Discharges (cubic feet per second)			
	Drainage Area	10-Percent-	2-Percent-	1-Percent-	0.2-Percent-
Flooding Source and Location Storay Crack East Tributary	(square nines)	Annual-Chance	Annual-Chance	Annual-Chance	Annual-Chance
At mouth	1 309	105	176	189	222
At mouth	1.509	105	170	109	
Storey Creek - Middle Tributary					
At mouth	1.323	100	165	176	206
Summer Creek	6.0	1.050	1.000	1.450	1 5 50
At mouth	6.2	1,050	1,300	1,450	1,750
At Southwest 135th Avenue	4.0	800	1,000	1,100	1,350
Tualatin River					
At rail road crossing	690.8	16,000	26,900	33,500	48,400
At Farmington	550.9	13,800	23,200	29,000	41,800
DS of Rock creek confluence	548.6	13,700	23,100	28,900	41,700
DS of Dairy Creek confluence	462.0	12,100	20,300	25,400	36,700
DS of Golf Course Tributory	221.4	7,400	12,400	15,500	22,400
Upper end of the Tualatin River	214.3	7,200	12,100	15,200	21,900
Tualatin River - Golf Course Overflow					
At mouth	NA	1,665	2,970	3,859	5,285
Tualatin River - LaFolette Overflow					
At mouth	NA	978	1,711	2,056	3,387
Turner Creek					
At mouth	2.0	320	406	441	522
Waihle Creek					
At mouth	12.0	1 045	1 692	1 815	2 1 1 3
At NW Groveland Drive (Highway 26)	3 2	180	234	297	380
At NW West Union Road	2.0	112	161	222	349
Waible Creek - Unwi Tributary					
At mouth	12	220	362	387	443
At Brookwood Parkway	1.0	173	208	266	387
Weikle Couch Weikedem <sup>1</sup> 2					
At mouth	0.4	15	56	66	80
At mouth	0.4	43	30	00	00

		Peak Discharges (cubic feet per second)			
	Drainage Area	10-Percent-	2-Percent-	1-Percent-	0.2-Percent-
Flooding Source and Location	(square miles)	Annual-Chance	Annual-Chance	Annual-Chance	Annual-Chance
Waible Creek Vributary''4					
At mouth	0.5	49	86	92	109
At NW West Union Road	0.4	33	47	54	56
Wapato Creek					
At mouth	22.0	650	1,150	1,400	2,000
At Washington/Yamhill County Line	13.0	550	850	1,000	1,350
West Fork Dairy Creek					
At Banks Road	46	4,200	6,090	7,010	9,630
Willow Creek					
At mouth	5.1	799	1,022	1,115	1,328
At Northwest 173rd Avenue	2.6	432	547	595	704

# 3.2 Hydraulic Analyses

Analyses of the hydraulic characteristics of flooding from the sources studied were carried out to provide estimates of the elevations of floods of the selected recurrence intervals. Users should be aware that flood elevations shown on the FIRM represent rounded whole-foot elevations and may not exactly reflect the elevations shown on the Flood Profiles or in the Floodway Data tables in the FIS report. Flood elevations shown on the FIRM are primarily intended for flood insurance rating purposes. For construction and/or floodplain management purposes, users are cautioned to use the flood elevation data presented in this FIS in conjunction with the data shown on the FIRM.

Many flooding sources discussed in sections below have been revised with new revised studies. Refer to Section 10 – Revision Descriptions for details.

Hydraulic analyses for all streams studied in detail were performed using the USACE HEC-2 step-backwater computer program (Reference 16). Cross-section data used in the program came from a number of sources. Cross sections are composites of data from USACE field surveys, city topographic maps (References 17 though 21), the USGS topographic information. All bridges, dams, and culverts were field checked to obtain elevation data and structural geometry.

Digital methods were used wherever possible to reduce redundant work effort and automate the direct transfer of data. They were used to directly convert a network of sections and alignments into section positions and distances, to convert survey data to the model cross sections, and to automatically map the 1- and 0.2-percent annual chance floodplain boundaries based on widths from the model output and to use those same data for the Floodway Data tables in a spreadsheet.

Water-surface profile computations at bridges are based on present normal bridge openings. Consideration was not given either to the possible blockage of bridge openings by sediment and debris or to future bridge enlargement.

Field surveys were made to establish stream channel profiles, cross sections, and a few high-water elevations for approximately 13.5 miles of Fanno Creek, 1.5 miles of Ash Creek, and 2.1 miles of Summer Creek. The original field surveys began in September 1997 and were completed in March 1998. Additional field surveyed cross sections on both Fanno Creek and Ash Creek were obtained by crews from the Cities of Beaverton

and Tigard and Washington County, Oregon, during the winter months of 1998-99.

The model for Unnamed Tributary of McKay Creek was calibrated using engineering judgment and information about past flooding events from local officials and residents along the Unnamed Tributary. Numerous high water marks from the January 31, 1987 flood were used in the model calibration for the entire 1.8-mile study reach.

Locations of selected cross sections used in the hydraulic analyses are shown on the Flood Profiles (Exhibit 1). For stream segments for which a floodway was computed (Section 4.2), selected cross-section locations are also shown on the FIRM. Where appropriate, backwater elevations from the Tualatin River were shown on the final Flood Profiles for Fanno Creek.

Hydraulic roughness (Manning's "n" values) for the channel and overbanks were first estimated from field observations. The "n" values were then adjusted to match high-water marks where available. Tabulated "n" values are shown in Table 4 for all streams studied in detail.

# Table 4. Roughness Coefficient - Manning's "n" Values

Stream	<u>Overbank</u>	<u>Channel</u>
Ash Creek	0.040 - 0.180	0.030 - 0.065
Real Creek	0.02 - 0.07	0.030 - 0.003
Beauerton Creek	0.02 - 0.07	0.07 - 0.08
Bethany Creek	0.001 - 0.200	0.012 - 0.030
Bronson Creek	0.055 - 0.000	0.033 - 0.040
Butternut Creek	0.03 0.07	0.04 - 0.11
Cadar Creak	0.03 - 0.07	0.03 - 0.07
Cedar Mill Creek and tributaries	0.02 0.25	0.030 - 0.000
Celabrity	0.02 - 0.25	0.02 - 0.08
Chicken Creek and West Tributery	0.02 0.10	0.05
Council Creek	0.02 - 0.10	0.02 - 0.10
Dairy Creek	0.04 - 0.10	0.042 - 0.083
Dawson Creek	0.04 - 0.10	0.04 - 0.10
Deer Creek	0.00 - 0.10	0.035 - 0.035
Erickson Creek	0.030 0.065	0.035
Enerson Creek	0.030 - 0.005	0.03 - 0.03
Cales Creek	0.077 0.110	0.043 - 0.080
Glencoe Swale	0.077 - 0.110	0.030 - 0.055
Gordon Creek	0.04 - 0.06	0.030 - 0.055
Hall Creek and tributaries	0.04 = 0.00	0.033 - 0.030
Hadras Creak	0.02 0.10	0.02 - 0.09
Holcomb Creek	0.02 - 0.10	0.02 - 0.10
North Johnson Creek and tributaries	0.02 0.25	0.02 0.08
McKay Creek and Unnamed Tributary	0.02 - 0.25	0.02 - 0.03
Nyberg Slough	0.050 - 0.095	0.40 - 0.05
Rock Creek North	0.04 - 0.07	0.40 - 0.03
Rock Creek South	0.02 - 1.00	0.04 - 0.08
South Johnson Creek	0.02 - 1.00	0.04 - 0.08
Storey Creek and tributaries	0.03 - 0.10	0.00 0.00
Summer Creek	0.04 - 0.30	0.045 - 0.085
Tualatin River and overflows	0.063 - 0.120	0.047 - 0.050
Turner Creek	0.04 - 0.08	0.045 - 0.070
Waible Creek and tributaries	0.035 - 0.100	0.050 - 0.065
Wapato Creek	0.080 - 0.090	0.050 - 0.052
West Fork Dairy Creek	0.08 - 0.11	0.055 - 0.057
Willow Creek	0.04 - 0.08	0.030 - 0.065
	0.01 0.00	0.000 0.000

Overbank roughness factors were based on digital aerial orthophotographs flown in 1999 by Washington County (Reference 22). Base map references of similar roughness were identified electronically as an AutoCAD layer on the aerial orthophotographs. Geographic Information System techniques were used to compute the weighted average "n" values at each of the overbanks for the surveyed cross sections. Using the techniques described above, overbank roughness values ranged from 0.04 to 0.120.

Water-surface profile computations at bridges are based on present normal bridge openings. Consideration was not given either to the possible blockage of bridge openings by sediment and debris or to future bridge enlargement.

Starting water-surface elevations (WSELs) for the Tualatin River were obtained from a hydraulic analysis performed by the USACE for the West Linn FIS (Reference 23).

Starting WSELs for Ash Creek and Summer Creek were obtained from those modeled for Fanno Creek at the point of each creek's respective confluence. Starting WSELs for Fanno Creek were based on the slopearea method; backwater from the Tualatin River taken from the City of Durham FIS report (Reference 15) is reflected on the water-surface profiles.

Both upstream and downstream elevations for the Tualatin River Side Channel and Nyberg Slough were obtained from Tualatin River profiles located at the entrance and exit of the overbank channels. For Nyberg Slough, overflow from the Tualatin River does not reach the slough for floods with less than a 6.6-percent-annual-chance frequency. Thus, the 10percent-annual-chance flood is not shown on the profile for Nyberg Slough.

For all other steams studied in detail, starting WSELs were obtained using the normal-depth routine of the HEC-2 program.

Results of the hydraulic analyses for Council Creek showed that the 1percent-annual-chance flood elevations for the entire reach studied in the community are below the 1-percent-annual-chance flood elevation on Dairy Creek at its confluence with Council Creek as presented in the Washington County, Oregon, Flood Insurance Study (Reference 5). Therefore, the 1- and 0.2-percent-annual-chance flood elevations and boundaries along Council Creek, as presented on the profiles and maps, are the result of backwater from Dairy Creek.

Flood profiles were drawn showing computed WSELs to an accuracy of 0.5 foot for floods of the selected recurrence intervals (Exhibit 1).

Elevations along Wapato Creek and Rock Creek are controlled by Tualatin River during a 1-percent-annual-chance flood. The profiles for the creek reflect that analysis.

New 2-foot contour maps were developed by David Smith and Associates, Inc., for Ash Creek, Fanno Creek and Summer Creek. They are based on aerial photography flown in December 1997 (Reference 24).

Approximate flood boundaries were based upon the existing Flood Plain Delineation Maps (Reference 25) and Flood Hazard Boundary Map (FHBM) (Reference 26).

Because of stream meanders, distances on the FIRM, published separately, may not agree exactly with distances on the profiles (Exhibit 1).

The hydraulic analyses for this study were based on unobstructed flow. The flood elevations shown on the Flood Profiles (Exhibit 1) are thus considered valid only if hydraulic structures remain unobstructed, operate properly, and do not fail.

#### **3.3** Vertical Datum

All FIS reports and FIRMs are referenced to a specific vertical datum. The vertical datum provides a starting point against which flood, ground, and structure elevations can be referenced and compared. Until recently, the standard vertical datum used for newly created or revised FIS reports and FIRMs was the National Geodetic Vertical Datum of 1929 (NGVD). With the completion of the North American Vertical Datum of 1988 (NAVD), many FIS reports and FIRMs are now prepared using NAVD as the referenced vertical datum.

To accurately convert flood elevations from the current NGVD29 datum to the newer NAVD88 datum, the following procedure was implemented. Use CORPSCON to determine whether it is necessary to use a Stream-byStream or Countywide factor in the conversion. Using the FEMA protocol for determining the conversion factor (*FEMA Guidelines & Specifications* – *Appendix B*) the decision was made that a single, countywide conversion factor was acceptable to use in performing the datum conversion for Washington County, OR. The average datum conversion factor for Washington County is calculated to be +3.52 ft. The final NAVD88 elevations were computed by adding the calculated value to the existing NGVD29 data.

All previous elevations in Washington County have been converted from NGVD to NAVD by adding 3.52 feet. Flood elevations shown in this FIS report and on the FIRM are referenced to the NAVD.

Flood elevations shown in this FIS report and on the FIRM are referenced to NAVD. These flood elevations must be compared to structure and ground elevation referenced to the same vertical datum. For information regarding conversion between the NGVD and NAVD, visit the National Geodetic Survey website at <u>www.ngs.noaa.gov</u>, or contact the National Geodetic Survey at the following address:

NGS Information Services NOAA, N/NGS12 National Geodetic Survey SSMC-3, #9202 1315 East-West Highway Silver Spring, Maryland 20910-3282 (301) 713-3242 (301) 713-4172 (fax)

Temporary vertical monuments are often established during the preparation of a flood hazard analysis for the purpose of establishing local vertical control. Although these monuments are not shown on the FIRM, they may be found in the Technical Support Data Notebook associated with the FIS report and FIRM for this community. Interested individuals may contact FEMA to access these data.

To obtain current elevation, description, and/or location information for benchmarks shown on this map, please contact the Information Services Branch of the NGS at (301) 713-3242, or visit their website at <u>www.ngs.noaa.gov</u>.

# 4.0 FLOODPLAIN MANAGEMENT APPLICATIONS

The NFIP encourages State and local governments to adopt sound floodplain management programs. To assist in this endeavor, each FIS report provides 1-percent-annual-chance floodplain data, which may include a combination of the following: 10-, 2-, 1-, and 0.2-percent-annual-chance flood elevation; delineations of the 1- and 0.2-percent-annual-chance floodplains; and a 1-percent-annual-chance floodway. This information is presented on the FIRM and in many components of the FIS report, including Flood Profiles and Floodway Data tables. Users should reference the data presented in the FIS report as well as additional information that may be available at the local community map repository before making flood elevation and/or floodplain boundary determinations.

## 4.1 Floodplain Boundaries

To provide a national standard without regional discrimination, the 1percent-annual-chance flood has been adopted by FEMA as the base flood for floodplain management purposes. The 0.2-percent-annual-chance flood is employed to indicate additional areas of flood risk in the community. For each stream studied by detailed methods, the 1- and 0.2-percentannual-chance floodplain boundaries have been delineated using the flood elevations determined at each cross section. Between cross sections, the boundaries were interpolated using topographic maps at a scale of 1:4,800, and 1:2,400 with contour intervals of 2 feet and 4 feet (References 18, 19, 20, and 21).

The 1- and 0.2-percent-annual-chance floodplain boundaries are shown on the FIRM. On this map, the 1-percent-annual-chance floodplain boundary corresponds to the boundary of the areas of special flood hazards (Zones A and AE), and the 0.2-percent-annual-chance floodplain boundary corresponds to the boundary of areas of moderate flood hazards. In cases where the 1- and 0.2-percent-annual-chance floodplain boundaries are close together, only the 1-percent-annual-chance floodplain boundary has been shown. Small areas within the floodplain boundaries may lie above the flood elevations, but cannot be shown due to limitations of the map scale and/or lack of detailed topographic data.

The approximate 1-percent-annual-chance flood boundaries were obtained from the Floodplain Delineation Maps published by Washington County (Reference 25) and the FHBM for Washington County (Reference 26).

The approximate 1-percent-annual-chance floodplain boundaries for Hedges Creek were delineated on a topographic map at a scale of 1:24,000, with a contour interval of 10 feet (Reference 27).
For the streams studied by approximate methods, only the 1-percentannual-chance floodplain boundary is shown on the FIRM.

## 4.2 Floodways

Encroachment on floodplains, such as structures and fill, reduces floodcarrying capacity, increases flood heights and velocities, and increases flood hazards in areas beyond the encroachment itself. One aspect of floodplain management involves balancing the economic gain from floodplain development against the resulting increase in flood hazard. For purposes of the NFIP, a floodway is used as a tool to assist local communities in this aspect of floodplain management. Under this concept, the area of the 1-percent-annual-chance floodplain is divided into a floodway and a floodway fringe. The floodway is the channel of a stream, plus any adjacent floodplain areas, that must be kept free of encroachment so that the base flood can be carried without substantial increases in flood heights. Minimum Federal standards limit such increases to 1 foot, provided that hazardous velocities are not produced. The floodways in this study are presented to local agencies as minimum standards that can be adopted directly or that can be used as a basis for additional floodway studies.

The floodways presented in this study were computed for certain stream segments on the basis of equal-conveyance reduction from each side of the floodplain. Floodway widths were computed at cross sections. Between cross sections, the floodway boundaries were interpolated. The results of the floodway computations are tabulated for selected cross section (see Table 5, Floodway Data). In cases where the floodway and 1-percent-annual-chance floodplain boundaries are either close together or collinear, only the floodway boundary is shown.

The area between the floodway and 1-percent-annual-chance floodplain boundaries is termed the floodway fringe. The floodway fringe encompasses the portion of the floodplain that could be completely obstructed without increasing the water-surface elevation (WSEL) or the base flood more than 1 foot at any point. Typical relationships between the floodway and the floodway fringe and their significance to floodplain development are shown in Figure 1.



**Figure 1. Floodway Schematic** 

FLOODING S	OURCE		FLOODWAY		1-1	PERCENT-ANNU WATER SURFA	AL-CHANCE FLOO	DD				
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH (FEET)	SECTION AREA (SQ.FEET)	MEAN VELOCITY (FEET/SEC.)	REGULATORY (FEET NAVD)	WITHOUT FLOODWAY (FEET NAVD)	WITH FLOODWAY (FEET NAVD)	INCREASE (FEET)				
ASH CREEK		( /					, , ,	. ,				
A B C D E F G H I J K	0.10 0.19 0.33 0.41 0.55 0.72 0.91 1.08 1.28 1.39 1.52	60 26 116 96 70 106 66 50 18 36 56	301 147 716 440 229 441 180 248 129 158 238	3.4 7.0 1.3 2.1 4.0 1.9 4.7 3.1 5.6 4.6 2.7	164.1 164.1 164.2 164.9 166.0 167.9 173.3 177.5 180.6 184.5	160.5 <sup>2</sup> 162.5 <sup>2</sup> 164.1 164.2 164.9 166.0 167.9 173.3 177.5 180.6 184.5	161.4 <sup>2</sup> 162.8 <sup>2</sup> 164.8 164.9 165.6 166.7 168.8 174.3 178.4 181.5 185.1	0.9 0.3 0.7 0.7 0.7 0.9 1.0 0.9 0.9 0.6				
					FLOOD	WAY DATA						
	ORPORATED ARE	11, UK 45			ASH	ASH CREEK						

FLOODING S	OURCE		FLOODWAY		1-	PERCENT-ANNU WATER SURFA	AL-CHANCE FLOO	DD	
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH (FEET)	SECTION AREA (SQ.FEET)	MEAN VELOCITY (FEET/SEC.)	REGULATORY (FEET NAVD)	WITHOUT FLOODWAY (FEET NAVD)	WITH FLOODWAY (FEET NAVD)	INCREASE (FEET)	
BEAL CREEK		, , ,						. ,	
A B C D E F G H I	417 637 1,024 1,608 1,785 2,082 2,227 2,468 2,757	145 47 273 125 93 24 53 76 67	431 181 1,200 746 529 118 228 325 247	1.6 3.2 0.5 0.6 0.8 3.5 1.8 1.2 1.6	169.1 169.4 171.3 171.6 172.0 172.1 172.2	168.6 <sup>2</sup> 169.4 171.3 171.3 171.6 172.0 172.1 172.2	169.3 <sup>2</sup> 169.6 <sup>2</sup> 170.2 171.8 171.8 172.2 172.6 172.9 173.1	0.7 0.8 0.5 0.5 0.6 0.6 0.8 0.9	
evations computed without co	onsideration of backwate	r effects from Council	Creek						
		AGENCY	1						
WASHING		TY. OR			FLOOD	WAY DATA			
	DRPORATED ARE	AS		BEAL CREEK					

FLOODING SOURCE		FLOODWAY			1-PERCENT-ANNUAL-CHANCE FLOOD WATER SURFACE ELEVATION			
		WIDTH	SECTION	MEAN	REGULATORY	WITHOUT	WITH	INCREASE
CROSS SECTION	DISTANCE <sup>1</sup>		AREA	VELOCITY		FLOODWAY	FLOODWAY	
		(FEET)	(SQ.FEET)	(FEET/SEC.)	(FEET NAVD)	(FEET NAVD)	(FEET NAVD)	(FEET)
BEAVERTON CREEK								
А	1,017	210	1,179	7.5	149.5	145.1 <sup>2</sup>	146.1 <sup>2</sup>	1.0
В	1.411	90	737	10.6	149.5	148.5 <sup>2</sup>	148.7 <sup>2</sup>	0.2
С	1,918	214	2,248	3.4	150.1	150.1	151.0	0.9
D	2,885	225	2,042	3.8	150.6	150.6	151.5	0.9
E	3,469	214	2,040	3.4	151.2	151.2	152.1	0.9
F	4,172	158	1,832	3.5	152.1	152.1	152.9	0.8
G	4,643	188	2,076	3.4	152.5	152.5	153.3	0.8
Н	4,881	189	2,164	2.7	152.6	152.6	153.4	0.8
I	5,501	161	1,682	4.1	152.9	152.9	153.8	0.9
J	5,667	172	1,957	3.6	153.6	153.6	154.4	0.8
K	5,941	190	2,217	3.0	153.8	153.8	154.6	0.8
L	6,388	193	2,195	3.5	154.0	154.0	154.9	0.9
Μ	6,501	71	918	6.8	155.5	155.5	155.8	0.3
Ν	7,041	190	2,565	2.7	156.6	156.6	157.1	0.5
0	7,386	200	2,636	1.9	156.7	156.7	157.1	0.4
Р	7,870	195	2,632	2.5	156.8	156.8	157.3	0.5
Q	8,519	204	2,537	2.6	156.9	156.9	157.5	0.6
R	9,367	198	2,718	2.4	157.1	157.1	157.8	0.7
S	10,104	198	2,561	2.2	157.3	157.3	158.0	0.7
Т	10,576	270	3,367	2.0	157.4	157.4	158.2	0.8
U	11,391	329	3,870	1.5	157.5	157.5	158.4	0.9
V	12,068	300	3,716	1.8	158.0	158.0	158.8	0.8
W	13,094	240	2,508	2.4	158.0	158.0	158.9	0.9
Х	13,970	230	2,422	2.5	158.2	158.2	159.1	0.9
Y	14,307	220	2,306	2.5	158.3	158.3	159.2	0.9
Z	14,753	216	2,121	2.8	158.5	158.5	159.4	0.9

<sup>2</sup>Elevations computed without consideration of backwater effects from Rock Creek North

ТАВ		FLOODWAY DATA
LE 5	AND INCORPORATED AREAS	BEAVERTON CREEK

FLOODING SOURCE		FLOODWAY			1-PERCENT-ANNUAL-CHANCE FLOOD WATER SURFACE ELEVATION			
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH	SECTION AREA	MEAN VELOCITY	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE
		(FEET)	(SQ.FEET)	(FEET/SEC.)	(FEET NAVD)	(FEET NAVD)	(FEET NAVD)	(FEET)
BEAVERTON CREEK								
AA	15,159	214	2,395	2.4	158.7	158.7	159.6	0.9
AB	15,551	220	2,306	2.7	158.8	158.8	159.8	1.0
AC	15,936	220	2,283	2.6	159.0	159.0	159.9	0.9
AD	16,368	120	1,225	5.1	159.3	159.3	160.1	0.8
AE	16,554	156	1,824	3.3	160.0	160.0	160.8	0.8
AF	17,052	158	1,816	3.2	160.2	160.2	161.0	0.8
AG	17,214	209	2,411	2.4	161.1	161.1	162.0	0.9
AH	18,009	215	2,497	2.4	161.2	161.2	162.2	1.0
Al	18,324	184	2,156	2.8	161.3	161.3	162.3	1.0
AJ	18,630	198	2,251	2.9	161.5	161.5	162.4	0.9
AK	18,926	190	2,212	2.6	161.5	161.5	162.5	1.0
AL	19,473	169	2,099	2.7	161.7	161.7	162.7	1.0
AM	20,062	226	1,959	2.9	162.0	162.0	162.9	0.9
AN	21,311	285	2,545	2.2	162.3	162.3	163.3	1.0
AO	21,903	276	2,331	2.4	162.4	162.4	163.4	1.0
AP	22,411	213	1,975	2.3	162.6	162.6	163.6	0.9
AQ	22.864	187	2.241	1.9	162.8	162.8	163.8	0.9
AR	23,366	166	1,764	2.9	163.0	163.0	163.9	0.9
AS	23,533	69	791	5.5	163.1	163.1	164.0	0.9
AT	24,090	281	2,549	2.2	164.0	164.0	164.8	0.8
AU	24,594	254	2,100	2.8	164.1	164.1	164.9	0.8
AV	26,374	83	602	9.3	164.7	164.7	165.4	0.7
AW	27,108	213	1,715	3.3	166.9	166.9	167.3	0.4
AX	27,789	224	1,832	3.5	167.2	167.2	167.6	0.4
AY	28,237	264	2,008	3.1	167.4	167.4	167.7	0.3
Α7	28 773	251	1 762	37	167.6	167.6	167.9	03

7	FEDERAL EMERGENCY MANAGEMENT AGENCY				
B					
	WASHINGTON COUNTT, OK				
сл	AND INCORPORATED AREAS	DEAVERION CREEK			

FLOODING SO	OURCE		FLOODWAY			1-PERCENT-ANNUAL-CHANCE FLOOD WATER SURFACE ELEVATION			
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH	SECTION AREA	MEAN VELOCITY	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE	
		(FEET)	(SQ.FEET)	(FEET/SEC.)	(FEET NAVD)	(FEET NAVD)	(FEET NAVD)	(FEET)	
BEAVERTON CREEK									
BA	30,064	327	1,959	3.5	167.8	167.8	168.2	0.4	
BB	31,158	241	1,331	4.6	168.3	168.3	168.6	0.3	
BC	31,555	64	520	8.8	168.7	168.7	168.8	0.1	
BD	31,751	112	876	6.7	170.0	170.0	170.2	0.2	
BE	32,190	199	1,700	3.1	170.3	170.3	171.2	0.9	
BF	32,458	186	1,362	4.8	170.3	170.3	171.2	0.9	
BG	33,321	332	2,531	1.7	170.7	170.7	171.6	0.9	
BH	33,852	339	2,378	1.6	170.7	170.7	171.6	0.9	
BI	34,114	243	2,264	1.6	170.8	170.8	171.7	0.9	
BJ	34,661	204	2,069	1.7	170.8	170.8	171.7	0.9	
ВК	35,077	207	1,959	1.8	170.9	170.9	171.8	0.9	
BL	35,351	211	2,033	1.7	170.9	170.9	171.8	0.9	
BM	35,580	205	1,924	1.8	170.9	170.9	171.8	0.9	
BN	36,047	203	1,953	2.0	171.0	171.0	171.9	0.9	
во	36,530	213	2,013	1.8	171.0	171.0	171.9	0.9	
BP	37,255	117	1,089	2.5	171.1	171.1	172.0	0.9	
BQ	37,487	127	1,221	3.0	171.2	171.2	172.0	0.8	
BR	37,868	135	735	3.7	171.4	171.4	172.2	0.8	
BS	38,285	382	3,522	1.0	171.9	171.9	172.9	1.0	
BT	39,137	211	1,824	1.5	171.9	171.9	172.9	1.0	
BU	39,433	98	712	2.7	171.9	171.9	172.8	0.9	
BV	39,765	82	1,118	1.7	172.6	172.6	173.5	0.9	
BW	40,440	90	832	2.2	172.7	172.7	173.6	0.9	
BX	40,624	70	837	1.9	173.2	173.2	174.1	0.9	
BY	40.845	84	671	3.4	173.2	173.1	174.0	0.9	
BZ	41,120	77	637	3.5	173.2	173.2	174.1	0.9	

TAE	FEDERAL EMERGENCY MANAGEMENT AGENCY	FLOODWAY DATA
3LE 5	WASHINGTON COUNTY, OR AND INCORPORATED AREAS	BEAVERTON CREEK

FLOODING SC	DURCE		FLOODWAY		1-1	PERCENT-ANNU/ WATER SURFA	AL-CHANCE FLOO CE ELEVATION	DD
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH	SECTION AREA	MEAN VELOCITY	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE
		(FEET)	(SQ.FEET)	(FEET/SEC.)	(FEET NAVD)	(FEET NAVD)	(FEET NAVD)	(FEET)
BEAVERTON CREEK								
CA	41,285	86	264	5.9	173.2	173.2	174.0	0.8
CB	41,535	96	520	3.0	174.8	174.8	175.6	0.8
CC	41,898	120	1,514	1.4	177.4	177.4	178.0	0.6
CD	42,010	60	587	2.6	177.4	177.4	178.0	0.6
CE	42,363	60	582	2.7	177.4	177.4	178.1	0.7
CF	42,547	53	519	3.0	177.6	177.6	178.3	0.7
CG	42,653	80	753	2.0	177.7	177.7	178.4	0.7
СН	43,303	181	1,269	1.3	177.8	177.8	178.5	0.7
CI	43,417	181	1,270	1.3	177.8	177.8	178.5	0.7
CJ	43,569	175	1,467	1.7	178.1	178.1	179.1	1.0
СК	44,047	176	1,443	1.8	178.1	178.1	179.1	1.0
CL	44,963	187	1,347	1.2	178.2	178.2	179.2	1.0
СМ	45,438	46	414	3.6	178.2	178.2	179.1	0.9
CN	45,632	65	457	3.3	178.5	178.5	179.4	0.9
CO	46,148	134	698	2.1	179.5	179.5	180.2	0.7
CP	46,252	53	452	3.5	179.5	179.5	180.2	0.7
CQ	46,810	63	491	3.1	179.7	179.7	180.5	0.8
CR	46,949	61	503	2.9	179.9	179.9	180.8	0.9
CS	47,249	91	797	1.9	180.0	180.0	180.9	0.9
СТ	47,459	146	1,857	0.8	180.1	180.1	181.0	0.9
CU	48,022	35	485	2.9	180.2	180.2	181.1	0.9
CV	48,402	95	618	2.4	180.5	180.5	181.5	1.0
CW	48,694	103	653	4.2	180.6	180.6	181.4	0.8
CX	49,093	46	105	1.4	182.2	182.2	182.9	0.7
CY	49,415	65	180	0.8	182.3	182.3	182.9	0.6
CZ	49,688	30	121	0.2	182.3	182.3	182.9	0.6

1	FEDERAL EMERGENCY MANAGEMENT AGENCY				
B		FLOODWAT DATA			
б	AND INCORPORATED AREAS	BEAVERION CREEK			

FLOODING SC	FLOODING SOURCE		FLOODWAY		1-	PERCENT-ANNU/ WATER SURFA	AL-CHANCE FLOG	DD
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH	SECTION AREA	MEAN VELOCITY	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE
		(FEET)	(SQ.FEET)	(FEET/SEC.)	(FEET NAVD)	(FEET NAVD)	(FEET NAVD)	(FEET)
BEAVERTON CREEK								
DA	49,807	30	15	1.3	182.7	182.7	182.9	0.2
DB	50,296	13	5	3.7	183.3	183.3	183.4	0.1
DC	50,513	82	315	0.1	183.3	183.3	183.7	0.4
DD	50,857	39	150	0.1	183.3	183.3	183.7	0.4
DE	51,109	34	144	0.1	183.3	183.3	183.7	0.4
DF	51,446	115	627	0.7	183.3	183.3	183.7	0.4
DG	51,730	45	255	1.3	183.4	183.4	183.7	0.3
DH	52,007	34	178	1.9	183.4	183.4	183.8	0.4
DI	52,457	28	349	0.5	189.1	189.1	189.5	0.4
DJ	52,670	25	324	0.7	189.1	189.1	189.5	0.4
DK	52,780	32	303	0.8	189.1	189.1	189.5	0.4
DL	53,025	30	59	2.4	189.1	189.1	189.6	0.5
DM	53,626	30	26	5.3	195.6	195.6	195.8	0.2
DN	53,795	30	26	5.3	196.9	196.9	197.3	0.4
DO	54,275	30	27	5.0	200.2	200.2	200.6	0.4
DP	54,598	89	59	5.6	203.2	203.2	203.3	0.1
DQ	54.946	105	52	5.3	208.5	208.5	208.6	0.1
DR	55.219	30	67	2.1	208.8	208.8	209.0	0.2
DS	55.483	30	128	1.1	208.8	208.8	209.1	0.3
DT	55,702	9	80	2.1	208.8	208.8	209.1	0.3
DU	56,057	69	200	1.7	208.8	208.8	209.3	0.5
DV	56,143	63	260	1.3	208.8	208.8	209.4	0.6
DW	56,362	17	44	3.9	208.9	208.9	209.3	0.4
DX	56,513	15	63	3.0	210.6	210.6	211.5	0.9
DY	56,796	13	44	4.4	211.4	211.4	212.2	0.8
DZ	56,883	23	18	5.1	215.6	215.6	215.8	0.2

Τ.	FEDERAL EMERGENCY MANAGEMENT AGENCY				
AB		FEOODWAY DATA			
Ē	WASHINGTON COUNTY, OR				
5	AND INCORPORATED AREAS	BEAVERION CREEK			

FLOODING SC	DURCE		FLOODWAY		1-PERCENT-ANNUAL-CHANCE FLOOD WATER SURFACE ELEVATION					
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH (FEET)	SECTION AREA (SQ.FEET)	MEAN VELOCITY (FEET/SEC.)	REGULATORY (FEET NAVD)	WITHOUT FLOODWAY (FEET NAVD)	WITH FLOODWAY (FEET NAVD)	INCREASE (FEET)		
BEAVERTON CREEK						, , ,				
EA EB EC ED EE EF EG EH EI EJ EK EL EM EN EO EP	56,987 57,104 57,389 57,711 57,794 57,958 59,692 59,945 60,121 60,420 60,531 60,725 60,916 61,362 61,511 61,774	30 31 36 14 11 24 56 23 20 6 6 8 16 6 7 7	26 35 53 74 74 92 377 72 46 20 21 18 65 11 23 28	3.5 2.6 1.7 1.2 2.3 1.8 0.2 1.1 1.7 3.9 3.7 4.3 1.3 7.4 3.5 2.8	216.2 216.8 218.8 222.3 222.3 244.9 245.1 245.4 247.0 247.3 250.5 259.1 260.4 264.0 266.6	216.2 216.8 218.8 222.3 222.3 224.9 245.1 245.4 247.0 247.3 250.5 259.1 260.4 264.0 266.6	216.4 217.0 219.0 222.9 223.1 245.0 245.2 245.5 247.2 247.4 251.0 259.4 260.4 264.7 267.4	0.2 0.2 0.6 0.6 0.8 0.1 0.1 0.1 0.2 0.1 0.5 0.3 0.0 0.7 0.8		
FEDERAL EMERG	ENCY MANAGEMENT	AGENCY	T							
WASHINGT	ON COUN	TY. OR			FLOOD	WAY DATA				
	RPORATED ARE	AS		BEAVERTON CREEK						

CROSS SECTION         DISTANCE <sup>1</sup> WIDTH (FEET)         SECTION AREA (SO.FEET)         MEAN VELOCITY (FEET NAVD)         REGULATORY (FEET NAVD)         WITHOUT FLOODWAY (FEET NAVD)         WITH FLOODWAY (FEET NAVD)           BETHANY CREEK                     FLOODWAY         (FEET NAVD)         (FEET NAVD)         (FEET NAVD)         (FEET NAVD)         (FEET NAVD)         (FEET NAVD)	FLOODING SOL	URCE		FLOODWAY		1-F	PERCENT-ANNUA WATER SURFA	AL-CHANCE FLOC	D
BETHANY CREEK         A         351         279         1,382         0.4         173.5         172.5 <sup>2</sup> 173.3 <sup>2</sup> B         675         279         1,507         0.3         173.5         172.5 <sup>2</sup> 173.3 <sup>2</sup> C         1,250         182         989         0.5         173.5         172.5 <sup>2</sup> 173.3 <sup>2</sup> D         1,907         20         98         5.2         173.5         172.5 <sup>2</sup> 173.3 <sup>2</sup> F         3,449         41         115         4.0         176.5         177.5         175.9         176.8           F         3,449         41         115         4.0         176.5         177.5         175.9         176.8         177.5         176.8         177.5         175.9         176.8         176.5         177.5         175.9         176.8         176.5         177.5         175.9         176.8         181.3         181.3         181.5         181.3         181.3         181.5         182.6         182.6         182.6         182.6         182.6         182.6         182.6         183.3         15.5         167.5         177.9         175.9         187.9         187.9         187.9         187.9<	CROSS SECTION	DISTANCE <sup>1</sup>	ICE <sup>1</sup> WIDTH (FEET)	SECTION AREA (SQ.FEET)	MEAN VELOCITY (FEET/SEC.)	REGULATORY (FEET NAVD)	WITHOUT FLOODWAY (FEET NAVD)	WITH FLOODWAY (FEET NAVD)	INCREASE (FEET)
A       351       279       1,382       0.4       173.5       172.5 <sup>2</sup> 173.3 <sup>2</sup> B       675       279       1,507       0.3       173.5       172.5 <sup>2</sup> 173.3 <sup>2</sup> C       1,250       182       989       0.5       173.5       172.5 <sup>2</sup> 173.3 <sup>2</sup> D       1,907       20       98       5.2       173.5       173.4 <sup>2</sup> 173.6 <sup>2</sup> E       2,917       60       158       3.3       175.9       175.9       176.5       177.5         G       4,110       40       145       3.4       180.9 </td <td>BETHANY CREEK</td> <td></td> <td></td> <td>, , , , , , , , , , , , , , , , , , ,</td> <td>· · · · ·</td> <td> /</td> <td>· · · · ·</td> <td></td> <td></td>	BETHANY CREEK			, , , , , , , , , , , , , , , , , , ,	· · · · ·	/	· · · · ·		
	A B C D E F G H I J K L	351 675 1,250 1,907 2,917 3,449 4,110 4,558 4,764 5,105 5,618 5,946 S,946	279 279 0 182 7 20 7 60 9 41 0 40 8 56 4 33 5 40 8 39 6 44	1,382 1,507 989 98 158 115 145 154 122 86 70 40	0.4 0.3 0.5 5.2 3.3 4.0 3.4 2.5 3.8 5.6 3.1 5.8	173.5 173.5 173.5 175.9 176.5 180.9 181.3 181.8 182.6 184.7 187.9	$172.5^{2}$ $172.5^{2}$ $173.4^{2}$ $175.9$ $176.5$ $180.9$ $181.3$ $182.6$ $184.7$ $187.9$	173.3 <sup>2</sup> 173.3 <sup>2</sup> 173.6 <sup>2</sup> 176.8 177.5 180.9 181.5 182.6 183.3 185.0 187.9	0.8 0.8 0.2 0.9 1.0 0.0 0.2 0.8 0.7 0.3 0.0
			GEMENT AGENCY						
WASHINGTON COUNTY, OR	WASHINGT	ON COUNT	DUNTY, OR			FLOOD	WAY DATA		

FLOODING SC	OURCE	FLOODWAY			1-PERCENT-ANNUAL-CHANCE FLOOD WATER SURFACE ELEVATION			
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH	SECTION AREA	MEAN VELOCITY	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE
		(FEET)	(SQ.FEET)	(FEET/SEC.)	(FEET NAVD)	(FEET NAVD)	(FEET NAVD)	(FEET)
BRONSON CREEK								
А	419	145	443	2.0	158.0	151.5 <sup>2</sup>	151.5 <sup>2</sup>	0.0
В	751	85	274	2.4	158.0	151.9 <sup>2</sup>	152.2 <sup>2</sup>	0.3
С	977	18	261	3.8	160.3	160.3	160.9	0.6
D	1,483	190	1,760	0.6	160.4	160.4	161.2	0.8
Е	1,776	225	1,774	0.6	160.5	160.5	161.2	0.7
F	2,053	191	1,134	0.7	160.5	160.5	161.2	0.7
G	2,326	199	995	0.8	160.6	160.6	161.2	0.6
Н	2,619	157	645	1.3	160.7	160.7	161.3	0.6
I	3,148	130	491	1.5	161.1	161.1	161.6	0.5
J	3,681	125	410	2.2	161.7	161.7	162.2	0.5
K	3,947	113	284	3.0	162.4	162.4	162.8	0.4
L	4,009	60	237	3.3	167.3	167.3	167.8	0.5
М	4,598	81	544	1.4	167.7	167.7	168.2	0.5
Ν	5,179	139	696	1.4	167.8	167.8	168.7	0.9
0	5,968	34	234	2.8	172.0	172.0	172.0	0.0
Р	6,155	58	410	1.7	172.5	172.5	173.3	0.8
Q	6,540	133	1,351	0.5	172.6	172.6	173.3	0.7
R	6,878	85	314	2.3	172.6	172.6	173.3	0.7
S	7,266	85	529	1.3	172.8	172.8	173.7	0.9
Т	7,486	30	196	3.4	173.1	173.1	173.9	0.8
U	7,727	80	519	1.2	173.6	173.6	174.3	0.7
V	7,954	20	90	7.2	173.6	173.6	174.3	0.7
W	8,166	40	177	3.8	176.8	176.8	177.0	0.2
Х	8,545	175	1,023	0.6	178.2	178.2	178.8	0.6
Y	8,805	199	793	0.8	183.3	183.3	183.5	0.2
Z	9,283	266	1,468	0.4	183.3	183.3	183.6	0.3

<sup>2</sup>Elevations computed without consideration of backwater effects from Beaverton Creek

ТАВ		FLOODWAY DATA
LE 5	AND INCORPORATED AREAS	BRONSON CREEK

FLOODING SC	DURCE	FLOODWAY			1-PERCENT-ANNUAL-CHANCE FLOOD WATER SURFACE ELEVATION			
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH	SECTION AREA	MEAN VELOCITY	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE
		(FEET)	(SQ.FEET)	(FEET/SEC.)	(FEET NAVD)	(FEET NAVD)	(FEET NAVD)	(FEET)
BRONSON CREEK								
AA	9,660	196	1,049	0.6	183.3	183.3	183.6	0.3
AB	10,101	236	1,878	0.3	185.0	185.0	185.3	0.3
AC	10,422	130	914	0.7	185.0	185.0	185.3	0.3
AD	10,764	24	135	4.6	185.0	185.0	185.2	0.2
AE	10,966	21	162	4.4	187.2	187.2	187.6	0.4
AF	11,260	76	563	1.2	187.2	187.2	188.1	0.9
AG	11,712	65	223	3.2	187.7	187.7	188.5	0.8
AH	11,880	36	152	4.5	188.3	188.3	188.9	0.6
AI	12,114	20	115	5.7	192.7	192.7	193.3	0.6
AJ	12,244	52	327	1.9	194.3	194.3	194.6	0.3
AK	12,333	106	630	1.3	194.9	194.9	195.7	0.8
AL	12,534	162	843	0.9	195.0	195.0	195.7	0.7
AM	12,902	172	693	1.1	195.1	195.1	195.8	0.7
AN	13,149	161	518	1.6	195.2	195.2	196.0	0.8
AO	13,518	118	380	1.5	195.6	195.6	196.5	0.9
AP	13,979	115	227	2.5	197.1	197.1	197.6	0.5
AQ	14,303	118	356	1.7	198.0	198.0	198.6	0.6
AR	15,312	126	308	2.1	199.8	199.8	200.8	1.0
AS	15,464	132	310	2.2	200.6	200.6	201.6	1.0
AT	15,757	114	318	2.4	201.8	201.8	202.8	1.0
AU	16,548	113	290	2.3	204.4	204.4	205.2	0.8
AV	16,802	134	361	1.6	205.1	205.1	206.0	0.9
AW	17,402	161	336	2.2	206.6	206.6	207.6	1.0
AX	17,846	163	236	3.3	209.1	209.1	210.0	0.9
AY	18,225	97	235	2.5	212.2	212.2	213.2	1.0
AZ	18,477	70	228	3.1	213.6	213.6	214.4	0.8

7	FEDERAL EMERGENCY MANAGEMENT AGENCY	ΕΙ ΟΟΡΨΑΥ ΠΑΤΑ
BLI	WASHINGTON COUNTY, OR	
сл	AND INCORPORATED AREAS	BRONSON CREEK

FLOODING SC	DURCE	FLOODWAY			1-PERCENT-ANNUAL-CHANCE FLOOD WATER SURFACE ELEVATION			
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH	SECTION AREA	MEAN VELOCITY	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE
		(FEET)	(SQ.FEET)	(FEET/SEC.)	(FEET NAVD)	(FEET NAVD)	(FEET NAVD)	(FEET)
BRONSON CREEK								
BA	19,047	97	310	1.9	216.7	216.7	217.3	0.6
BB	19,314	104	282	1.6	217.0	217.0	217.9	0.9
BC	19,741	89	213	2.1	218.2	218.2	219.2	1.0
BD	20,519	142	360	1.5	220.7	220.7	221.7	1.0
BE	20,946	26	81	6.5	223.1	223.1	223.9	0.8
BF	21,117	44	105	5.0	225.0	225.0	225.5	0.5
BG	21,674	92	282	1.9	227.4	227.4	228.4	1.0
BH	22,346	151	279	2.0	229.0	229.0	229.9	0.9
BI	22,974	172	255	1.5	232.7	232.7	233.2	0.5
BJ	23,737	224	326	1.1	237.3	237.3	237.3	0.0
BK	24,134	26	71	5.5	238.2	238.2	239.0	0.8
BL	24,705	40	148	2.9	243.4	243.4	244.2	0.8
BM	25,210	50	132	3.3	246.2	246.2	246.6	0.4
BN	25,470	56	136	3.6	247.9	247.9	248.5	0.6
BO	25,871	80	166	2.4	249.6	249.6	250.2	0.6
BP	26,223	149	248	2.0	250.3	250.3	251.4	1.1
BQ	26,398	17	53	6.2	251.1	251.1	252.1	1.0
BR	26,734	90	228	1.6	255.0	255.0	255.5	0.5
BS	27,268	18	55	6.0	256.2	256.2	257.2	1.0
BT	27,968	31	117	2.8	264.1	264.1	264.3	0.2
BU	28,532	120	207	2.3	266.7	266.7	267.0	0.3
BV	28,736	39	106	3.4	272.4	272.4	272.6	0.2

FEDERAL EMERGENCY MANAGEMENT AGENCY WASHINGTON COUNTY, OR AND INCORPORATED AREAS

FLOODWAY DATA
BRONSON CREEK

FLOODING SO	URCE		FLOODWAY		1-1	PERCENT-ANNU/ WATER SURFA	AL-CHANCE FLOG	DD
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH	SECTION AREA	MEAN VELOCITY	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE
		(FEET)	(SQ.FEET)	(FEET/SEC.)	(FEET NAVD)	(FEET NAVD)	(FEET NAVD)	(FEET)
BUTTERNUT CREEK								
А	971	27	111	9.1	144.3	125.5 <sup>2</sup>	125.9 <sup>2</sup>	0.4
В	1,193	88	638	2.0	144.3	133.3 <sup>2</sup>	133.4 <sup>2</sup>	0.1
С	1.891	49	344	2.8	144.3	133.5 <sup>2</sup>	133.5 <sup>2</sup>	0.0
D	3,023	169	454	2.8	144.3	134.2 <sup>2</sup>	134.6 <sup>2</sup>	0.4
Е	3.976	107	318	3.8	144.3	135.9 <sup>2</sup>	136.3 <sup>2</sup>	0.4
F	4,505	101	326	3.2	144.3	$137.0^{2}$	137.9 <sup>2</sup>	0.9
G	5.376	91	274	3.9	144.3	$139.4^{2}$	140.3 <sup>2</sup>	0.9
Н	6.023	74	207	5.2	144.3	$141.5^{2}$	$142.5^2$	1.0
	6 698	80	288	37	144.3	$143.8^2$	$144.5^2$	0.7
J	6.882	72	719	1.3	150.7	150.7	151.4	0.7
ĸ	7,450	88	773	1.2	150.7	150.7	151.5	0.8
L	8,584	99	717	1.4	150.7	150.7	151.6	0.9
М	9,293	97	574	1.8	150.8	150.8	151.7	0.9
Ν	9,447	50	399	2.5	151.1	151.1	152.1	1.0
0	10,251	77	512	2.0	151.5	151.5	152.5	1.0
Р	11,130	44	197	4.3	152.1	152.1	153.1	1.0
Q	11,679	89	419	2.3	153.6	153.6	154.4	0.8
R	12,503	85	372	2.4	154.2	154.2	155.2	1.0
S	13,904	68	219	4.0	157.5	157.5	158.3	0.8
Т	14,725	70	286	2.8	160.9	160.9	161.5	0.6
U	15,861	61	211	4.4	163.3	163.3	164.2	0.9
V	16,842	46	204	3.8	166.5	166.5	166.9	0.4
W	17,104	51	240	3.4	167.0	167.0	167.5	0.5
Х	17,378	58	439	1.3	170.5	170.5	171.4	0.9
Y	17,706	69	480	1.1	170.6	170.6	171.5	0.9
Z	17,942	70	404	1.8	170.7	170.7	171.6	0.9

<sup>1</sup>Feet above confluence with Tualatin River

<sup>2</sup>Elevations computed without consideration of backwater effects from Tualatin River

FEDERAL EMERGENCY MANAGEMENT AGENCY WASHINGTON COUNTY, OR AND INCORPORATED AREAS
FLOODWAY DATA
BUTTERNUT CREEK

FLOODING SC	DURCE		FLOODWAY			1-PERCENT-ANNUAL-CHANCE FLOOD WATER SURFACE ELEVATION			
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH	SECTION AREA	MEAN VELOCITY	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE	
		(FEET)	(SQ.FEET)	(FEET/SEC.)	(FEET NAVD)	(FEET NAVD)	(FEET NAVD)	(FEET)	
BUTTERNUT CREEK									
AA	18,222	64	190	3.8	171.1	171.1	171.8	0.7	
AB	18,906	91	451	1.5	172.3	172.3	173.0	0.7	
AC	19,059	55	287	2.4	173.1	173.1	173.5	0.4	
AD	19,340	54	254	2.9	173.5	173.5	173.9	0.4	
AE	19,850	70	177	4.7	174.9	174.9	175.3	0.4	
AF	20,452	24	95	4.6	177.2	177.2	177.8	0.6	
AG	20,933	25	118	4.0	179.5	179.5	180.1	0.6	
AH	21,396	32	125	3.7	180.7	180.7	181.7	1.0	
AI	21,945	36	124	3.6	182.9	182.9	183.8	0.9	
AJ	22,200	45	208	2.0	185.1	185.1	186.0	0.9	
AK	22,384	54	191	2.2	185.4	185.4	186.3	0.9	
AL	22,964	12	40	10.6	187.5	187.5	188.0	0.5	
AM	23,466	27	88	5.1	192.3	192.3	193.3	1.0	
AN	24,440	23	118	2.3	195.4	195.4	195.6	0.2	
AO	24,666	20	75	3.9	195.5	195.5	195.8	0.3	
AP	25,050	18	68	4.2	196.3	196.3	197.3	1.0	
AQ	25,448	38	113	1.6	197.7	197.7	198.2	0.5	
AR	25,601	33	113	1.6	198.7	198.7	199.1	0.4	
AS	25,799	20	85	2.2	198.8	198.8	199.3	0.5	
AT	25,881	23	81	2.3	199.0	199.0	199.4	0.4	
AU	26,063	31	123	1.5	199.5	199.5	200.5	1.0	
AV	26,502	49	146	1.4	199.9	199.9	200.8	0.9	
AW	26,728	48	236	0.7	199.9	199.9	200.8	0.9	
AX	26,909	16	50	3.1	200.1	200.1	201.1	1.0	
	20,000				200.1	200.1	20111		

<sup>1</sup>Feet above confluence with Tualatin River

Ţ	FEDERAL EMERGENCY MANAGEMENT AGENCY	FLOODWAY DATA			
B					
		BUTTERNUT CREEK			
сл	AND INCORPORATED AREAS				

FLOODING S	OURCE		FLOODWAY		1-	PERCENT-ANNU WATER SURFA	AL-CHANCE FLOO	
			SECTION	MEAN		WITHOUT	WITH	
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH	AREA	VELOCITY	REGULATORY	FLOODWAY	FLOODWAY	INCREASE
		(FEET)	(SQ.FEET)	(FEET/SEC.)	(FEET NAVD)	(FEET NAVD)	(FEET NAVD)	(FEET)
CEDAR CREEK								
А	445	20	148	6.5	144.2	139.3 <sup>2</sup>	139.9 <sup>2</sup>	0.6
В	939	40	227	5.4	144.2	$143.4^{2}$	143.9 <sup>2</sup>	0.5
С	1.319	40	305	4.3	145.2	145.2	145.6	0.4
D	1.682	100	625	2.1	145.8	145.8	146.2	0.4
Е	2.125	65	423	3.1	146.1	146.1	146.5	0.4
F	2,440	60	386	3.3	146.4	146.4	146.9	0.5
G	2,964	57	378	3.0	147.2	147.2	147.7	0.5
H	3,190	50	518	2.2	150.2	150.2	150.7	0.5
I	3,588	151	1,232	1.1	150.6	150.6	151.2	0.6
J	3,958	125	943	1.5	150.6	150.6	151.2	0.6
К	4,584	70	517	2.6	150.9	150.9	151.5	0.6
L	5,291	61	516	1.7	151.5	151.5	152.1	0.6
Μ	5,646	32	441	2.0	156.8	156.8	157.4	0.6
Ν	6,789	82	763	2.1	157.6	157.6	158.2	0.6
0	7,311	130	1,334	1.4	157.8	157.8	158.4	0.6
Р	8,229	135	990	2.0	158.1	158.1	158.7	0.6
Q	9,142	82	559	2.9	158.9	158.9	159.4	0.5
R	9,731	38	331	4.5	160.4	160.4	160.8	0.4
S	9,913	96	855	1.5	162.0	162.0	162.9	0.9
Т	10,462	195	1,567	1.3	162.1	162.1	163.0	0.9
U	10,824	168	1,353	1.4	162.2	162.2	163.1	0.9
V	11,560	141	617	3.0	162.6	162.6	163.6	1.0
W	12,407	189	1,178	1.5	163.8	163.8	164.4	0.6
Х	12,767	42	756	2.1	173.6	173.6	174.2	0.6
Y	13,440	86	1,303	1.0	173.7	173.7	174.4	0.7
Z	14,785	58	693	1.8	173.7	173.7	174.6	0.9
AA	14,886	170	1,011	1.7	175.4	175.4	175.7	0.3
AB	15,431	242	2,483	1.0	175.5	175.5	175.8	0.3

<sup>2</sup>Elevations computed without consideration of backwater effects from Chicken Creek

ТАВ		FLOODWAY DATA
LE 5	AND INCORPORATED AREAS	CEDAR CREEK

FLOODING SC	DURCE		FLOODWAY		1-PERCENT-ANNUAL-CHANCE FLOOD WATER SURFACE ELEVATION				
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH	SECTION AREA	MEAN VELOCITY	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE	
		(FEET)	(SQ.FEET)	(FEET/SEC.)	(FEET NAVD)	(FEET NAVD)	(FEET NAVD)	(FEET)	
CEDAR MILL CREEK									
А	720	176	476	3.3	170.7	168.9 <sup>2</sup>	169.6 <sup>2</sup>	0.7	
В	1.309	130	472	3.4	170.7	170.8	171.7	0.9	
Ċ	1,680	163	639	3.0	171.4	171.4	172.5	1.1	
D	2,500	177	591	3.2	172.8	172.8	173.7	0.9	
Е	3,458	293	456	3.2	173.7	173.7	174.6	0.9	
F	3,796	44	393	3.6	181.1	181.1	181.1	0.0	
G	4,106	40	399	3.4	181.1	181.1	181.6	0.5	
Н	4,418	198	1,304	1.1	181.1	181.1	181.8	0.7	
I	4,815	326	1,907	0.7	181.2	181.2	181.9	0.7	
J	5,163	301	736	2.4	182.1	182.1	182.4	0.3	
К	5,723	52	403	3.3	182.2	182.2	182.6	0.4	
L	6,062	91	644	1.9	182.7	182.7	183.3	0.6	
М	6,216	56	422	2.7	182.8	182.8	183.4	0.6	
Ν	6,600	77	551	2.1	183.0	183.0	183.7	0.7	
0	7,283	127	615	2.1	183.4	183.4	184.0	0.6	
Р	7,435	98	410	3.2	183.5	183.5	184.1	0.6	
Q	7,705	100	395	3.7	184.0	184.0	184.5	0.5	
R	7,979	124	642	2.0	184.4	184.4	185.0	0.6	
S	8,218	173	735	1.8	184.5	184.5	185.2	0.7	
Т	8,448	153	847	1.8	184.9	184.9	185.4	0.5	
U	8,652	181	956	1.2	184.9	184.9	185.5	0.6	
V	8,961	64	266	4.8	186.0	186.0	186.0	0.0	
W	9,310	80	468	1.6	188.8	188.8	189.7	0.9	
Х	9,651	90	392	2.2	188.9	188.9	189.8	0.9	
Y	9,896	96	317	2.4	189.2	189.2	190.1	0.9	
Z	10,161	60	221	3.3	191.0	191.0	191.7	0.7	

<sup>2</sup>Elevations computed without consideration of backwater effects from Beaverton Creek

TAB		FLOODWAY DATA
LE 5	AND INCORPORATED AREAS	CEDAR MILL CREEK

FLOODING SC	DURCE		FLOODWAY		1-PERCENT-ANNUAL-CHANCE FLOOD WATER SURFACE ELEVATION				
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH	SECTION AREA	MEAN VELOCITY	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE	
		(FEET)	(SQ.FEET)	(FEET/SEC.)	(FEET NAVD)	(FEET NAVD)	(FEET NAVD)	(FEET)	
CEDAR MILL CREEK									
AA	10,496	31	154	4.7	194.6	194.6	194.6	0.0	
AB	10,683	55	180	4.7	195.9	195.9	196.2	0.3	
AC	11,213	31	184	4.0	198.3	198.3	199.1	0.8	
AD	11,440	58	186	4.7	198.9	198.9	199.9	1.0	
AE	11,740	60	168	5.3	201.9	201.9	202.5	0.6	
AF	12,247	29	215	3.4	204.7	204.7	205.6	0.9	
AG	13,193	19	101	4.7	207.7	207.1	207.7	0.6	
AH	13,629	20	112	4.2	210.0	210.0	210.0	0.0	
AI	13,787	27	84	5.6	212.4	212.3	212.4	0.1	
AJ	13,897	30	203	2.3	213.0	213.0	213.0	0.0	
AK	14,316	31	169	4.1	213.8	213.7	213.8	0.1	
AL	14,823	29	202	3.5	215.4	215.1	215.4	0.3	
AM	15,007	19	104	6.1	216.0	215.4	216.0	0.6	
AN	15,250	18	118	5.3	218.2	217.7	218.2	0.5	
AO	15,639	20	137	4.6	220.9	220.6	220.9	0.3	
AP	15,851	8	80	7.9	224.0	223.4	224.0	0.6	
AQ	16,173	34	233	2.7	225.3	224.9	225.3	0.4	
AR	16,540	69	264	2.4	227.6	226.7	227.6	0.9	
AS	16,746	17	124	5.1	229.0	228.5	229.0	0.5	
AT	16,880	46	240	2.9	229.7	228.9	229.7	0.8	
AU	17,053	145	299	2.8	232.7	231.8	232.7	0.9	
AV	17,712	19	109	6.4	234.2	233.7	234.2	0.5	
AW	18,405	29	179	4.0	239.4	239.0	239.4	0.4	
AX	18,853	32	144	5.7	242.2	241.4	242.2	0.8	
AY	19,549	45	193	3.6	248.7	247.7	248.7	1.0	
AZ	20,008	25	124	5.6	252.5	252.2	252.5	0.3	

٦٢,	FEDERAL EMERGENCY MANAGEMENT AGENCY	
B		FLOODWAT DATA
сл	AND INCORPORATED AREAS	

FLOODING SC	DURCE		FLOODWAY		1-PERCENT-ANNUAL-CHANCE FLOOD WATER SURFACE ELEVATION				
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH (EEET)	SECTION AREA (SQ FEFT)	MEAN VELOCITY (FEET/SEC.)	REGULATORY	WITHOUT FLOODWAY (FEET NAVD)	WITH FLOODWAY (FEET NAVD)	INCREASE (FEET)	
CEDAR MILL CREEK		(1 = 1 )					(122110/02)	(1 2 2 1)	
BA BB BC BD BE BF BG BH BI	20,278 20,395 20,793 21,460 21,641 21,851 22,052 22,199 22,453	78 59 82 60 44 21 18 24 126	363 381 355 161 176 72 89 154 195	2.0 1.7 2.1 4.9 4.0 8.2 6.5 3.5 4.3	280.4 280.5 280.8 282.3 283.3 284.5 288.7 292.7 300.3	280.1 280.2 280.3 282.0 282.7 284.2 287.7 291.9 300.3	280.4 280.5 280.8 282.3 283.3 284.5 288.7 292.7 300.3	0.3 0.5 0.3 0.6 0.3 1.0 0.8 0.0	
FEDERAL EMERG		AGENCY			FLOOD	WAY DATA			
	ON COUN	ΓY, OR			CEDAR	MILL CREEK			

FLOODING SC	DURCE		FLOODWAY		1-	PERCENT-ANNU WATER SURFA	AL-CHANCE FLOO	DD
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH (FEET)	SECTION AREA (SQ.FEET)	MEAN VELOCITY (FEET/SEC.)	REGULATORY (FEET NAVD)	WITHOUT FLOODWAY (FEET NAVD)	WITH FLOODWAY (FEET NAVD)	INCREASE (FEET)
CEDAR MILL CREEK NORTH OVERFLOW A B C D E	83 336 427 799 1,133	(FEET) 169 35 31 24 104	(SQ.FEET) 340 62 37 34 67	(FEET/SEC.) 0.7 3.7 6.2 6.8 3.4	(FEET NAVD) 206.6 207.2 208.0 210.9 211.9	(FEET NAVD) 206.6 207.2 208.0 210.9 211.9	(FEET NAVD) 207.3 207.8 208.1 211.0 212.2	(FEET) 0.7 0.6 0.1 0.1 0.3
eet above confluence with Ced	ar Mill Creek		1	1	1		1 1	
					FLOOD	WAY DATA		
	ON COUN	AS		CED		EK NORTH OV	ERFLOW	

FLOODING SC	DURCE		FLOODWAY		1-PERCENT-ANNUAL-CHANCE FLOOD WATER SURFACE ELEVATION				
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH	SECTION AREA	MEAN VELOCITY	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE	
		(FEET)	(SQ.FEET)	(FEET/SEC.)	(FEET NAVD)	(FEET NAVD)	(FEET NAVD)	(FEET)	
CELEBRITY CREEK									
А	326	21	94	2.2	179.2	179.2	179.9	0.7	
В	526	14	60	3.4	179.6	179.6	180.2	0.6	
С	710	7	41	6.3	179.9	179.9	180.6	0.7	
D	1,020	19	73	2.8	181.5	181.5	181.7	0.2	
E	1,134	21	97	2.1	182.0	182.0	182.6	0.6	
F	1,445	18	84	2.4	182.4	182.4	182.9	0.5	
G	1,568	19	58	3.5	183.1	183.1	183.7	0.6	
Н	1,714	21	88	2.3	183.6	183.6	184.1	0.5	
Ι	1,917	19	77	2.6	183.8	183.8	184.3	0.5	
J	2,070	19	65	3.1	184.2	184.2	184.7	0.5	
К	2,328	13	46	4.4	186.4	186.4	186.7	0.3	
L	2,517	18	55	3.1	187.7	187.7	188.0	0.3	
М	2,666	21	94	1.8	188.6	188.6	189.1	0.5	
Ν	2,796	19	53	3.3	188.8	188.8	189.5	0.7	
0	3,115	20	48	5.2	191.7	191.7	192.7	1.0	
Р	3,431	23	51	4.7	194.2	194.2	195.1	0.9	
Q	3,718	19	47	4.2	195.6	195.6	196.5	0.9	
R	3,939	12	35	4.4	197.2	197.2	197.6	0.4	
S	4,074	12	37	4.0	197.8	197.8	198.6	0.8	
Т	4,255	12	38	3.9	199.1	199.1	200.1	1.0	
U	4,459	12	35	4.9	201.2	201.2	201.4	0.2	
V	4,831	23	37	5.0	204.5	204.5	204.7	0.2	
W	5,215	14	24	7.0	206.1	206.1	206.4	0.3	
Х	5,550	25	34	4.9	211.8	211.8	211.8	0.0	

FEDERAL EMERGENCY MANAGEMENT AGENCY WASHINGTON COUNTY, OR AND INCORPORATED AREAS
FLOODWAY DATA
CELEBRITY CREEK

FLOODING SO	FLOODWAY	FLOODWAY WATER SURFACE ELEVATION							
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH (FEET)	SECTION AREA (SQ.FEET)	MEAN VELOCITY (FEET/SEC.)	REGULATORY (FEET NAVD)	WITHOUT FLOODWAY (FEET NAVD)	WITH FLOODWAY (FEET NAVD)	INCREASE (FEET)	
CHICKEN CREEK									
А	2,316	45	381	4.1	134.4	132.0 <sup>3</sup>	132.5 <sup>3</sup>	0.5	
В	2,540	93	409	3.9	134.4	134.0 <sup>3</sup>	134.1 <sup>3</sup>	0.1	
С	3,065	117	596	2.9	134.9	134.9	135.0	0.1	
D	4,074	110	694	3.5	135.9	135.9	136.1	0.2	
E	7,110	130	634	4.1	139.5	139.5	139.9	0.4	
F	7,299	57	363	5.7	141.1	141.1	141.2	0.1	
G	8,632	50	473	4.0	144.1	144.1	144.8	0.7	
Н	11,383	109	305	4.8	149.6	149.6	150.4	0.8	
I	12,425	165	1,119	1.9	151.0	151.0	151.6	0.6	
J	13,121	200	1,105	1.4	151.2	151.2	151.9	0.7	
К	13,273	67	581	2.1	153.8	153.8	154.5	0.7	
L	14,049	92	632	1.8	153.8	153.8	154.6	0.8	
Μ	15,132	70	356	4.1	154.1	154.1	154.8	0.7	
Ν	15,243	92	239	4.6	157.2	157.2	158.0	0.8	
CHICKEN CREEK WEST TRIBUTARY									
A	751 <sup>2</sup>	32	185	3.1	153.3	153.3	154.1	0.8	
В	$1.512^{2}$	32	140	32	156.3	156.3	157 1	0.8	
Feet above confluence with Tuala	atin River								
Feet above confluence with Chicl	ken Creek								
Elevations computed without con	sideration of backwater	effects from Tualatin	River						
FEDERAL EMERGE		AGENCY			FLOOD	WAY DATA			

FLOODING SC	DURCE		FLOODWAY		1-PERCENT-ANNUAL-CHANCE FLOOD WATER SURFACE ELEVATION				
		WIDTH	SECTION	MEAN		WITHOUT	WITH	INCREASE	
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH	AREA	VELOCITY	REGULATORT	FLOODWAY	FLOODWAY	INCINEAGE	
		(FEET)	(SQ.FEET)	(FEET/SEC.)	(FEET NAVD)	(FEET NAVD)	(FEET NAVD)	(FEET)	
COUNCIL CREEK									
А	2,783	248	1,107	1.9	156.3	143.3 <sup>2</sup>	144.1 <sup>2</sup>	0.8	
В	3,662	298	1,196	1.4	156.3	143.6 <sup>2</sup>	144.5 <sup>2</sup>	0.9	
С	4.250	63	285	5.9	156.3	143.6 <sup>2</sup>	144.6 <sup>2</sup>	1.0	
D	4,432	57	310	5.8	156.3	146.7 <sup>2</sup>	146.9 <sup>2</sup>	0.2	
E	5.015	97	792	2.5	156.3	148.2 <sup>2</sup>	149.0 <sup>2</sup>	0.8	
F	7.942	166	1.074	1.6	156.3	149.6 <sup>2</sup>	150.6 <sup>2</sup>	1.0	
G	8.348	164	968	2.6	156.3	149.9 <sup>2</sup>	150.8 <sup>2</sup>	0.9	
Н	8.543	71	482	3.6	156.3	$150.5^{2}$	151.3 <sup>2</sup>	0.8	
I	8.958	128	779	1.7	156.3	$151.1^{2}$	152.0 <sup>2</sup>	0.9	
J	10.928	172	968	1.5	156.3	151.9 <sup>2</sup>	152.6 <sup>2</sup>	0.7	
К	13,467	44	339	4.9	156.3	153.7 <sup>2</sup>	154.3 <sup>2</sup>	0.6	
L	13,968	114	658	2.8	156.3	$155.3^{2}$	155.9 <sup>2</sup>	0.6	
М	16,971	139	1.052	1.9	156.3	155.8 <sup>2</sup>	156.5 <sup>2</sup>	0.7	
Ν	18,557	139	840	1.8	156.3	156.3	156.9	0.6	
0	19.373	39	408	4.4	157.1	157.1	157.8	0.7	
P	21,282	57	562	2.8	160.1	160.1	160.3	0.2	
Q	22,478	145	1,196	1.3	160.6	160.6	160.9	0.3	
R	22,671	106	727	2.1	160.8	160.8	161.1	0.3	
S	23,311	76	828	1.9	165.0	165.0	166.0	1.0	
Т	23,641	183	823	2.2	165.1	165.1	166.1	1.0	
U	24,727	169	869	1.9	165.5	165.5	166.5	1.0	
V	25,111	1/4	1,182	0.9	165.6	165.6	166.5	0.9	
VV ×	28,143	1/5	794	0.8	165.8	165.8	100.8	1.0	
A V	30,233 31 294	227	444 857	3.3 0.3	169.0	169.0	109.9	0.9	
7	32 610	221	149	29	172 1	172 1	170.2	0.9	

TABLE 5

<sup>2</sup>Elevations computed without consideration of backwater effects from Dairy Creek

FEDERAL EMERGENCY MANAGEMENT AGENCY WASHINGTON COUNTY, OR AND INCORPORATED AREAS

FLOODWAY DATA

COUNCIL CREEK

FLOODING SC	URCE		FLOODWAY		1-1	PERCENT-ANNU WATER SURFA	AL-CHANCE FLOO	DD		
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH (FEET)	SECTION AREA (SQ.FEET)	MEAN VELOCITY (FEET/SEC.)	REGULATORY (FEET NAVD)	WITHOUT FLOODWAY (FEET NAVD)	WITH FLOODWAY (FEET NAVD)	INCREASE (FEET)		
COUNCIL CREEK		, ,	, , ,	, , , , , , , , , , , , , , , , , , ,			· · · · · ·	. ,		
AA AB AC AD AE	33,061 33,727 34,070 35,087 35,235	120 103 82 116 101	778 627 486 519 389	0.7 0.8 0.3 0.3 0.3	172.1 172.2 172.2 172.2	172.1 172.2 172.2 172.2	172.9 173.0 173.0 173.0 173.0	0.8 0.9 0.8 0.8 0.8		
et above confluence with Dair	y Creek									
	ENCY MANAGEMENT	AGENCY	<u>г</u>							

		FLOODWAY	LOODWAY WATER SURFACE				E ELEVATION	
CROSS SECTION DISTANCE <sup>1</sup>	WIDTH (FEET)	SECTION AREA (SQ.FEET)	MEAN VELOCITY (FEET/SEC.)	REGULATORY (FEET NAVD)	WITHOUT FLOODWAY (FEET NAVD)	WITH FLOODWAY (FEET NAVD)	INCREASI (FEET)	
DAIRY CREEK								
A       3,512         B       5,485         C       9,167         D       9,713         E       11,136         F       11,438         G       11,842         H       12,157         I       14,863         J       16,220         K       19,998         L       24,827         M       27,542         N       29,088         O       32,530         P       33,566	984 1,222 345 661 380 370 1,078 1,362 1,576 1,587 1,624 1,362 770 1,437 1,017 1,036	15,983 17,350 6,445 10,203 5,003 6,628 20,232 12,460 29,815 21,143 22,317 20,267 9,691 10,703 10,678 10,309	1.4 1.7 6.8 3.3 7.9 4.1 1.2 2.9 0.5 0.9 0.9 0.8 1.6 1.0 0.4 1.5	152.3 152.3 153.1 153.7 155.6 156.0 156.1 156.3 156.3 156.3 156.3 156.4 156.6 156.9 158.9	152.3 152.3 153.1 153.7 155.6 156.0 156.1 156.3 156.3 156.3 156.3 156.4 156.6 156.9 158.9	153.1 153.2 154.1 154.6 154.7 156.4 156.9 157.0 157.2 157.2 157.2 157.3 157.4 157.7 158.0 159.7	0.8 0.9 1.0 0.9 1.0 0.8 0.9 0.9 0.9 0.9 0.9 1.0 1.0 1.1 1.1 0.8	
FEDERAL EMERGENCY MANAGEMENT	AGENCY	FLOODWAY DATA						

FLOODING S	OURCE		FLOODWAY		1-PERCENT-ANNUAL-CHANCE FLOOD WATER SURFACE ELEVATION				
			SECTION	MEAN		WITHOUT	WITH		
CROSS SECTION	DISTANCE <sup>1</sup>	VVIDTH	AREA	VELOCITY	REGULATORY	FLOODWAY	FLOODWAY	INCREASE	
		(FEET)	(SQ.FEET)	(FEET/SEC.)	(FEET NAVD)	(FEET NAVD)	(FEET NAVD)	(FEET)	
DAWSON CREEK									
А	398	143	573	3.3	147.1	137.3 <sup>2</sup>	138.3 <sup>2</sup>	1.0	
В	1,563	82	217	7.1	147.1	138.5 <sup>2</sup>	139.5 <sup>2</sup>	0.9	
С	1,959	45	289	4.9	147.1	$145.7^{2}$	145.7 <sup>2</sup>	0.0	
D	2,616	65	383	27	147 1	$146.2^2$	146 6 <sup>2</sup>	0.4	
Ē	3 277	80	325	39	147 1	146 7 <sup>2</sup>	147 3 <sup>2</sup>	0.6	
F	3 699	80	320	3.9	147.5	147.5	148.1	0.0	
Ġ	4,034	139	809	1.6	151.3	151.3	152.2	0.9	
Ĥ	4,602	160	846	1.3	151.4	151.4	152.3	0.9	
1	5,709	151	613	1.9	151.8	151.7	152.5	0.8	
J	6.366	70	286	3.3	152.3	152.3	153.0	0.7	
K	6,985	55	213	4.6	154.3	154.3	155.1	0.8	
L	7,343	54	254	2.9	155.0	155.0	156.0	1.0	
Μ	7,726	58	220	4.3	155.9	155.9	156.7	0.8	
Ν	8,397	93	321	4.3	158.2	158.2	159.0	0.8	
0	9,067	12	101	5.7	163.1	163.0	163.4	0.4	
Р	9,743	45	241	3.0	163.9	163.8	164.5	0.7	
Q	9,973	55	237	3.6	164.0	163.9	164.8	0.9	
R	10,291	95	351	2.6	164.3	164.3	165.3	1.0	
S	10,853	102	465	1.8	164.8	164.8	165.7	0.9	
Т	11,409	28	111	4.9	168.1	168.1	168.2	0.1	
U	11,586	79	342	2.5	169.8	169.8	170.8	1.0	
V	12,375	60	168	5.1	171.7	171.5	172.1	0.6	
W	12,715	50	153	4.0	172.9	173.0	173.8	0.8	
Х	12,955	44	150	4.4	173.7	173.7	174.7	1.0	
Y	13,426	75	183	3.8	176.0	176.0	176.4	0.4	
Z	14,649	42	153	2.1	181.0	181.0	181.4	0.4	
AA	15,630	80	226	2.4	182.6	182.5	183.6	1.1	
AB	16,130	70	163	2.6	183.9	184.0	184.7	0.7	

 $^{2}\mbox{Elevations}$  computed without consideration of backwater effects from Rock Creek North

ΤA	FEDERAL EMERGENCY MANAGEMENT AGENCY	FLOODWAY DATA
BLE	WASHINGTON COUNTY, OR	DAWSON CREEK
сл	AND INCORPORATED AREAS	DANGON GREEK

FLOODING S	OURCE		FLOODWAY		1-	PERCENT-ANNU WATER SURFA	AL-CHANCE FLO	DD
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH (FEET)	SECTION AREA (SQ.FEET)	MEAN VELOCITY (FEET/SEC.)	REGULATORY (FEET NAVD)	WITHOUT FLOODWAY (FEET NAVD)	WITH FLOODWAY (FEET NAVD)	INCREASE (FEET)
DEER CREEK		( )			,	,	, ,	( )
A B C D E F G H I	319 592 864 1,298 1,520 2,377 2,741 3,185 3,439	15 10 13 14 9 7 9 8	38 27 13 26 22 19 11 17 12	2.2 3.0 6.1 3.1 3.6 4.2 7.3 4.8 7.0	175.7 176.1 176.3 178.4 179.7 187.7 192.0 197.6 202.2	175.7 176.1 176.3 178.4 179.7 187.7 192.0 197.6 202.2	175.9 176.4 176.4 179.2 179.8 187.7 192.1 198.0 202.2	0.2 0.3 0.1 0.8 0.1 0.0 0.1 0.4 0.0
et above confluence with Bet	hany Creek							
					FLOOD	WAY DATA		
		11, UN AS			DEE			

FLOODING SC	DURCE		FLOODWAY		1-PERCENT-ANNUAL-CHANCE FLOOD WATER SURFACE ELEVATION			
			SECTION	MEAN		WITHOUT	WITH	
CROSS SECTION	DISTANCE <sup>1</sup>		AREA	VELOCITY	REGULATORY	FLOODWAY	FLOODWAY	INCREASE
		(FEET)	(SQ.FEET)	(FEET/SEC.)	(FEET NAVD)	(FEET NAVD)	(FEET NAVD)	(FEET)
ERICKSON CREEK								
А	379	34	122	4.3	172.6	168.9 <sup>2</sup>	169.4 <sup>2</sup>	0.5
В	680	27	91	5.3	172.6	170.4 <sup>2</sup>	170.7 <sup>2</sup>	0.3
С	1.023	17	90	4.4	172.6	$172.0^{2}$	$172.5^{2}$	0.5
D	1.412	28	209	1.9	173.3	173.3	174.0	0.7
Ē	1.626	26	156	2.8	173.4	173.4	174.2	0.8
F	1,874	67	235	2.2	173.7	173.7	174.4	0.7
G	2,270	31	69	2.7	177.8	177.8	178.3	0.5
H	2,527	40	35	5.4	181.9	181.9	182.4	0.5
I	2,773	40	148	1.3	182.2	182.2	183.0	0.8
J	3,346	24	46	4.1	187.7	187.7	187.7	0.0
К	3,799	41	35	5.4	188.6	188.6	189.1	0.5
L	4,289	39	58	3.2	189.6	189.6	190.2	0.6
Μ	4,658	35	96	2.0	190.8	190.8	191.0	0.2
Ν	5,009	21	143	1.5	190.8	190.8	191.1	0.3
0	5,297	19	67	3.1	190.8	190.8	191.2	0.4
Р	5,650	10	18	1.3	194.1	194.1	194.8	0.7
Q	5,914	9	22	1.0	194.5	194.5	195.5	1.0
R	6,215	5	18	1.7	197.3	197.3	198.0	0.7
S	6,452	7	10	5.9	198.0	198.0	198.9	0.9
Т	6,781	34	204	0.8	198.9	198.9	199.9	1.0
U	6,897	33	178	1.0	198.9	198.9	199.9	1.0
V	7,086	52	220	0.7	199.0	199.0	200.0	1.0
W	7,410	39	155	1.0	199.1	199.1	200.0	0.9
Х	7,617	40	147	1.2	199.2	199.2	200.1	0.9
Y	7,993	24	74	1.8	199.6	199.6	200.3	0.7
Z	8,330	15	41	3.9	200.2	200.2	200.8	0.6
AA	8,637	16	32	4.3	202.8	202.8	202.8	0.0

<sup>2</sup>Elevations computed without consideration of backwater effects from Beaverton Creek

TAB		FLOODWAY DATA
LE 5	AND INCORPORATED AREAS	ERICKSON CREEK

FLOODING SOURCE		FLOODWAY			1-PERCENT-ANNUAL-CHANCE FLOOD WATER SURFACE ELEVATION			
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH	SECTION AREA	MEAN VELOCITY	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE
		(FEET)	(SQ.FEET)	(FEET/SEC.)	(FEET NAVD)	(FEET NAVD)	(FEET NAVD)	(FEET)
FANNO CREEK								
А	0.02	251	2,242	1.9	130.8	120.8 <sup>2</sup>	121.8 <sup>2</sup>	1.0
В	0.20	351	2,723	1.6	130.8	$121.4^{2}$	$122.3^2$	0.9
С	0.53	411	2,308	1.8	130.8	$122.2^{2}$	$123.2^2$	1.0
D	0.99	221	1,218	3.5	130.8	126 7 <sup>2</sup>	$127.6^2$	0.9
Е	1.30	126	987	4.2	131.3	131.3	132.0	0.7
F	1.45	98	901	4.7	133.2	133.2	134.2	1.0
G	1.76	271	2,285	1.8	135.2	135.2	136.1	0.9
Н	2.25	281	1,770	2.4	136.6	136.6	137.6	1.0
I	2.73	191	793	5.2	141.0	141.0	141.4	0.4
J	3.02	301	2,048	2.0	142.2	142.2	142.7	0.5
K	3.43	311	2,417	1.7	143.8	143.8	144.7	0.9
L	3.80	301	876	4.7	145.3	145.3	146.2	0.9
Μ	4.08	256	1,206	3.4	147.8	147.8	148.5	0.7
Ν	4.41	410	1,825	2.2	149.4	149.4	150.0	0.6
0	4.91	161	789	5.1	155.9	155.9	156.8	0.9
Р	5.16	256	2,707	1.5	158.6	158.6	159.4	0.8
Q	5.73	331	2,447	1.6	159.5	159.5	160.3	0.8
R	5.99	201	1,998	1.9	161.6	161.6	162.2	0.6
S	6.25	191	1,649	2.0	162.3	162.3	163.2	0.9
Т	6.40	191	992	3.3	163.2	163.2	163.9	0.7
U	6.66	226	1,420	1.9	163.9	163.9	164.8	0.9
V	7.11	226	1,280	2.1	165.7	165.7	166.7	1.0
W	7.48	321	1,718	1.6	169.0	169.0	169.3	0.3
Х	7.75	331	1,570	1.5	169.5	169.5	170.0	0.5
Y	8.11	601	1,877	1.3	170.6	170.6	171.1	0.5
Z	8.29	351	1,120	2.1	171.8	171.8	172.7	0.9

<sup>1</sup>Miles above confluence with Tualatin River

<sup>2</sup>Elevations computed without consideration of backwater effects from Tualatin River

ТАВ		FLOODWAY DATA
LE 5	AND INCORPORATED AREAS	FANNO CREEK

	FLOODING SOURCE		FLOODWAY			WATER SURFACE ELEVATION			
CROSS SECTION DIS	STANCE <sup>1</sup>	WIDTH	SECTION AREA (SQ.FEET)	MEAN VELOCITY (FEET/SEC.)	REGULATORY	WITHOUT FLOODWAY (FEET NAVD)	WITH FLOODWAY (FEET NAVD)	INCREASE (FEET)	
FANNO CREEK		( )	(00. 227)	(	(	(	( )	( )	
AA AB AC AD AE AF AG AH AI AJ AJ AK AL AM AN AN AO AP AQ AR AR	8.67 8.91 9.42 9.55 9.97 10.17 10.62 10.76 11.03 11.38 11.58 11.87 12.18 12.36 12.81 13.16 13.32 13.49	206 95 311 96 146 141 76 151 190 176 206 141 236 96 91 76 80	1,364 605 1,194 529 1,490 806 549 871 1,234 493 425 532 315 863 346 498 360 416	1.6 3.7 1.9 4.2 1.4 2.5 3.6 2.3 1.6 4.0 4.5 3.6 5.9 1.8 3.7 2.6 3.5 3.1	180.7 182.1 186.1 189.0 192.2 194.1 198.0 201.0 204.0 207.8 210.7 214.4 220.0 221.1 230.8 236.4 239.1 240.3	180.7 182.1 186.1 189.0 192.2 194.1 198.0 201.0 204.0 207.8 210.7 214.4 220.0 221.1 230.8 236.4 239.1 240.3	181.0 182.5 186.6 189.7 193.2 194.8 199.0 201.8 204.8 208.3 211.3 215.4 220.3 222.1 231.8 237.4 239.8 241.3	0.3 0.4 0.5 0.7 1.0 0.7 1.0 0.8 0.8 0.5 0.6 1.0 0.3 1.0 1.0 1.0 1.0 1.0 1.0	
FEDERAL EMERGENCY M	ANAGEMENT AG	GENCY							
WASHINGTON	COUNT	í, or			FLOOD				

FLOODING S	OURCE		FLOODWAY		1-	PERCENT-ANNU WATER SURFA	AL-CHANCE FLOO	DD
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH	SECTION AREA	MEAN VELOCITY	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE
		(FEET)	(SQ.FEET)	(FEET/SEC.)	(FEET NAVD)	(FEET NAVD)	(FEET NAVD)	(FEET)
GALES CREEK								
А	0.80	2,000	4,233	2.4	167.3	162.3 <sup>2</sup>	163.2 <sup>2</sup>	0.9
В	1.49	1,500	3,744	2.7	167.7	167.7	168.5	0.8
С	1.64	900	6,145	1.6	169.4	169.4	170.3	0.9
D	1.88	1,620	8,828	1.1	171.8	171.8	172.5	0.7
Е	2.03	1,590	7,884	1.3	172.3	172.3	173.1	0.8
F	2.39	1,300	9,133	1.1	175.0	175.0	175.5	0.5
G	2.52	1,212	8,651	1.2	175.4	175.4	176.0	0.6
Н	2.98	1,950	11,580	0.9	175.6	175.6	176.3	0.7
I	3.35	2,000	7,884	1.3	175.8	175.8	176.5	0.7
J	4.18	410	1,199	8.3	178.5	178.5	179.3	0.8
K	4.28	180	1,951	5.1	182.7	182.7	182.9	0.2
L	4.38	350	2,727	3.6	183.6	183.6	183.9	0.3
М	4.98	2,120	9,893	1.0	184.9	184.9	185.9	1.0
Ν	5.20	2,450	7,252	1.4	185.2	185.2	186.2	1.0
0	5.68	2,370	5,147	1.9	186.8	186.8	187.7	0.9
Р	6.13	1,900	5,113	1.9	189.4	189.4	189.9	0.5
Q	6.51	1,600	3,240	3.0	191.4	191.4	192.4	1.0
R	6.93	1,260	3,861	2.5	196.8	196.8	197.8	1.0
S	7.16	660	4,170	2.3	198.8	198.8	199.5	0.7
Т	7.55	570	2,044	4.8	201.2	201.2	202.0	0.8
U	7.92	190	1,826	5.2	205.5	205.5	206.4	0.9
V	7.98	225	2,229	4.2	207.0	207.0	207.6	0.6
W	8.06	470	3,750	2.5	207.3	207.3	208.3	1.0
Х	8.42	350	3,469	2.7	208.9	208.9	209.8	0.9
Y	8.72	210	2,188	4.3	211.3	211.3	211.9	0.6
Z	8.98	350	2,632	3.6	214.4	214.4	215.1	0.7

<sup>1</sup>Miles above confluence with Tualatin River

<sup>2</sup>Elevations computed without consideration of backwater effects from Tualatin River

ТАВ		FLOODWAY DATA
LE 5	AND INCORPORATED AREAS	GALES CREEK

FLOODING S	OURCE		FLOODWAY		1-	PERCENT-ANNU WATER SURFA	AL-CHANCE FLOO	סכ
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH (FEET)	SECTION AREA (SQ.FEET)	MEAN VELOCITY (FEET/SEC.)	REGULATORY (FEET NAVD)	WITHOUT FLOODWAY (FEET NAVD)	WITH FLOODWAY (FEET NAVD)	INCREASE (FEET)
GALES CREEK								
AA AB AC AD AE AF AG	9.48 9.58 17.38 17.72 17.89 17.97 18.28	350 90 81 75 88 60 67	3,515 1,215 739 631 841 383 703	2.7 7.5 7.6 8.9 6.6 14.5 6.0	219.0 219.8 464.4 477.1 483.3 486.6 504.2	219.0 219.8 464.4 477.1 483.3 486.6 504.2	219.9 220.5 465.4 477.7 483.5 486.6 504.2	0.9 0.7 1.0 0.6 0.2 0.0 0.0
s above confluence with Tu	alatin River							
					FLOOD	WAY DATA		
	OBBORATED ADE	IY, OR			GALE	ES CREEK		

CROSS SECTION GLENCOE SWALE A B C	DISTANCE <sup>1</sup>	WIDTH (FEET)	SECTION AREA (SQ.FEET)	MEAN VELOCITY (FEET/SEC.)	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE
GLENCOE SWALE A B C	1,011	(FEET)	(SQ.FEET)	(FEET/SEC.)	(FEET NAVD)			
GLENCOE SWALE A B C	1,011				(* == * * * * * * = )	(FEET NAVD)	(FEET NAVD)	(FEET)
A B C	1,011							
B C	1 = 1 4	119	351	2.0	156.2	140.5 <sup>2</sup>	141.5 <sup>2</sup>	1.0
С	1,511	61	143	3.7	156.2	141.3 <sup>2</sup>	142.1 <sup>2</sup>	0.8
	2.038	40	125	3.8	156.2	143.0 <sup>2</sup>	143.7 <sup>2</sup>	0.7
D	2.647	22	104	3.6	156.2	$144.5^{2}$	$145.3^{2}$	0.8
Е	3,158	22	79	5.1	156.2	$146.5^{2}$	147.1 <sup>2</sup>	0.6
F	3,469	22	144	2.3	159.2	159.2	160.0	0.8
G	4,337	79	973	1.1	159.3	159.3	160.3	1.0
H	4,943	36	615	1.2	166.4	166.4	167.4	1.0
I	5,336	96	1,711	0.4	166.4	166.4	167.4	1.0
J	5,920	91	1,392	0.5	166.4	166.4	167.4	1.0
К	7,051	120	1,522	0.7	166.4	166.4	167.4	1.0
L	7,915	128	1,306	0.8	166.4	166.4	167.4	1.0
М	8,545	143	1,285	0.8	166.4	166.4	167.4	1.0
N	9,149	160	1,148	0.9	166.4	166.4	167.4	1.0
0	9,635	79	490	2.0	166.6	166.6	167.6	1.0
Р	10,051	71	411	2.3	166.8	166.8	167.7	0.9
Q	10,548	80	360	3.2	167.2	167.2	168.0	0.8
R	10,653	25	245	3.7	172.6	172.6	173.0	0.4
S	11,112	96	709	1.3	172.6	172.6	173.4	0.8
Т	11,598	54	271	2.6	172.7	172.7	173.5	0.8
U	12,055	109	344	2.5	173.2	173.2	173.8	0.6
V	12,680	48	91	5.1	173.3	173.3	173.7	0.4
W	13,235	39	179	2.6	175.6	175.6	175.9	0.3
Х	13,733	25	66	11.2	177.4	177.4	177.4	0.0
Y	14,329	67	305	2.4	183.7	183.7	184.3	0.6
Z	15,222	79	311	1.6	183.9	183.9	184.6	0.7

<sup>1</sup>Feet above confluence with McKay Creek

 $^{2}\mathsf{Elevations}$  computed without consideration of backwater effects from McKay Creek and Dairy Creek

TAB		FLOODWAY DATA
LE 5	AND INCORPORATED AREAS	GLENCOE SWALE

FLOODING SOURCE		FLOODWAY			1-PERCENT-ANNUAL-CHANCE FLOOD WATER SURFACE FLEVATION					
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH (FEET)	SECTION AREA (SQ.FEET)	MEAN VELOCITY (FEET/SEC.)	REGULATORY (FEET NAVD)	WITHOUT FLOODWAY (FEET NAVD)	WITH FLOODWAY (FEET NAVD)	INCREASE (FEET)		
GLENCOE SWALE		()	(0 4)	()	(	( ,	()	( )		
AA AB AC AD AE AF AG AH AI AJ AK AL et above confluence with McF	15,713 16,182 16,700 17,233 18,004 18,713 18,924 19,541 20,023 20,496 20,981 21,477	73 42 58 36 42 97 88 28 16 18 23 22	301 178 216 74 283 361 297 60 35 35 55 49	1.5 2.4 2.0 4.7 1.0 0.5 2.3 3.6 3.1 2.1 2.3	187.3 187.4 188.0 194.6 194.6 194.7 197.0 198.8 199.9 200.9	187.3 187.3 187.4 188.0 194.6 194.7 194.7 197.0 198.8 199.9 200.9	187.5 187.6 187.9 188.7 195.5 195.6 195.7 197.0 199.4 200.8 201.8	0.2 0.3 0.5 0.7 0.9 1.0 0.9 1.0 0.0 0.6 0.9 0.9		
FEDERAL EMERGENCY MANAGEMENT AGENCY			FLOODWAY DATA							
AND INCORPORATED AREAS			GLENCOE SWALE							

FLOODING SOURCE		FLOODWAY			1-PERCENT-ANNUAL-CHANCE FLOOD WATER SURFACE ELEVATION				
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH (FEET)	SECTION AREA (SQ.FEET)	MEAN VELOCITY (FEET/SEC.)	REGULATORY (FEET NAVD)	WITHOUT FLOODWAY (FEET NAVD)	WITH FLOODWAY (FEET NAVD)	INCREASE (FEET)	
GOLF CREEK		( )		( /	· · · · · · · · · · · · · · · · · · ·	<u> </u>	· · · · · · · · · · · · · · · · · · ·	. ,	
A B C D E F G H I J K L M N O P Q R	338 713 950 1,092 1,226 1,330 1,436 1,639 2,028 2,094 2,280 2,448 2,663 2,819 2,967 3,224 3,393 3,576	80 26 31 62 35 29 10 29 21 60 34 34 66 18 61 43 55 18	225 112 103 281 125 117 49 162 160 415 217 182 341 71 501 297 252 72	1.6 3.9 4.1 1.5 3.5 3.2 8.6 2.6 2.6 1.0 1.9 2.1 1.2 5.9 1.1 1.5 1.7 5.0	198.3 199.8 200.9 202.6 202.8 203.0 203.3 210.1 213.9 214.0 214.0 214.0 214.2 221.6 221.7 221.7 223.1	198.3 199.8 200.9 202.6 202.8 203.0 203.3 210.1 213.9 214.0 214.0 214.2 214.2 221.6 221.7 221.7 223.1	199.3 200.7 201.6 203.6 203.7 204.0 204.0 210.9 214.8 214.9 214.9 215.0 215.2 215.2 222.5 222.5 222.6 223.4	1.0 0.9 0.7 1.0 0.9 1.0 0.7 0.8 0.9 1.0 1.0 1.0 1.0 1.0 0.9 0.8 0.9 0.3	
FEDERAL EMERGENCY MANAGEMENT AGENCY			FLOODWAY DATA						
WASHINGTON COUNTY, OR									
FLOODING SC	DURCE		FLOODWAY		1-	PERCENT-ANNUA WATER SURFA	AL-CHANCE FLOO	DD	
--	---	--	---	--	--	---	--	--	
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH (FEET)	SECTION AREA (SQ.FEET)	MEAN VELOCITY (FEET/SEC.)	REGULATORY (FEET NAVD)	WITHOUT FLOODWAY (FEET NAVD)	WITH FLOODWAY (FEET NAVD)	INCREASE (FEET)	
GORDON CREEK									
A B C D E F G H I J K L M N O P	521 1,817 2,497 3,358 3,913 4,822 5,383 5,898 6,178 6,732 6,818 7,653 8,514 8,595 9,360 9,990 9,990	8 25 17 32 20 16 19 45 30 19 12 13 9 12 17 23	22 80 27 92 96 36 61 93 26 29 42 14 21 38 6 13	9.5 2.6 7.1 2.5 2.0 5.3 3.8 1.8 3.6 2.7 1.8 6.6 3.3 1.5 3.5 1.2	146.2 146.2 146.2 152.9 153.0 154.3 160.2 160.7 161.8 165.4 168.6 172.9 181.7 182.7 191.6 196.3	128.4 <sup>2</sup> 136.0 <sup>2</sup> 141.1 <sup>2</sup> 152.9 153.0 154.3 160.2 160.7 161.8 165.4 168.6 172.9 181.7 182.7 191.6 196.3	$128.5^2$ $136.7^2$ $141.1^2$ 153.6 153.9 154.7 160.4 161.4 161.8 165.5 168.6 172.9 182.6 183.5 191.6 196.3	0.1 0.7 0.9 0.4 0.2 0.7 0.0 0.1 0.0 0.0 0.9 0.8 0.0 0.0	
			r						
		AGENCY			FLOOD	WAY DATA			
		AS			GORD	ON CREEK			

FLOODING S	OURCE		FLOODWAY		1-PERCENT-ANNUAL-CHANCE FLOOD WATER SURFACE ELEVATION				
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH	SECTION AREA	MEAN VELOCITY	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE	
		(FEET)	(SQ.FEET)	(FEET/SEC.)	(FEET NAVD)	(FEET NAVD)	(FEET NAVD)	(FEET)	
HALL CREEK									
А	319	48	423	2.4	181.1	181.0	181.2	0.2	
В	641	31	264	2.8	181.1	181.1	181.2	0.1	
С	846	58	163	3.1	181.7	181.7	182.7	1.0	
D	1,184	116	304	1.6	182.1	182.1	183.1	1.0	
E	1,546	44	264	2.8	182.9	182.9	183.8	0.9	
F	1,906	93	725	1.0	183.8	183.8	184.8	1.0	
G	2,024	73	427	1.8	183.9	183.9	184.9	1.0	
Н	2,256	88	518	1.5	184.4	184.4	185.3	0.9	
I	2,491	64	352	2.1	184.6	184.6	185.4	0.8	
J	2,654	37	201	3.7	185.4	185.4	186.0	0.6	
К	2,807	226	627	1.3	185.8	185.8	186.3	0.5	
L	3,303	47	269	2.7	190.0	190.0	190.0	0.0	
М	3,747	15	137	5.0	191.3	191.3	191.8	0.5	
Ν	3,929	26	147	4.6	192.2	192.2	192.6	0.4	
0	4,133	24	168	4.0	193.4	193.4	194.3	0.9	
Р	4,339	73	298	2.1	194.5	194.5	195.4	0.9	
Q	4,603	71	389	1.9	195.1	195.1	195.9	0.8	
R	4,909	25	131	5.4	198.0	198.0	198.2	0.2	
S	5,264	126	552	0.5	198.4	198.4	199.4	1.0	
Т	5,551	126	469	0.6	198.4	198.4	199.4	1.0	
U	5,864	103	438	0.7	198.3	198.3	199.4	0.9	
V	6,148	13	51	4.9	198.5	198.5	199.4	0.9	
W	6,253	23	122	2.2	201.7	201.7	202.7	1.0	
Х	6,572	49	235	1.1	202.0	202.0	202.9	0.9	
Y	6,883	23	71	3.6	202.1	202.1	203.1	1.0	
Z	7.157	26	68	3.7	205.2	205.2	205.2	0.0	

<sup>1</sup>Feet above confluence with Beaverton Creek

ග AND INCORPORATED AREAS HALL CREEK	

FLOODING S	OURCE		FLOODWAY		WATER SURFACE ELEVATION				
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH	SECTION AREA	MEAN VELOCITY	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE	
		(FEET)	(SQ.FEET)	(FEET/SEC.)	(FEET NAVD)	(FEET NAVD)	(FEET NAVD)	(FEET)	
HALL CREEK									
AA	7,308	26	60	5.2	206.8	206.8	207.0	0.2	
AB	7,542	36	29	5.1	207.8	207.8	208.0	0.2	
AC	7,784	23	94	1.1	210.4	210.4	210.5	0.1	
AD	8,001	10	54	3.1	210.4	210.4	210.7	0.3	
AE	8,196	13	46	3.9	210.7	210.7	211.6	0.9	
AF	8,325	14	42	4.0	213.4	213.4	213.6	0.2	
AG	8,514	18	103	1.6	219.6	219.6	220.6	1.0	
AH	8,644	21	91	1.8	219.7	219.7	220.7	1.0	
AI	8,749	39	131	1.1	219.8	219.8	220.8	1.0	
AJ	8,921	22	61	2.7	220.1	220.1	220.9	0.8	
AK	9,111	15	30	5.0	222.0	222.0	222.0	0.0	
AL	9,295	55	231	0.7	227.3	227.3	228.1	0.8	
AM	9,536	19	38	4.3	227.3	227.3	228.0	0.7	
AN	9,846	13	35	5.3	231.9	231.9	231.9	0.0	
AO	9,966	9	32	5.2	235.8	235.8	236.2	0.4	
AP	10,091	15	45	3.9	236.1	236.1	237.0	0.9	
AQ	10,306	10	40	3.6	238.0	238.0	238.3	0.3	
AR	10,448	36	150	0.9	243.0	243.0	243.9	0.9	
AS	10,681	21	64	2.4	243.0	243.0	244.0	1.0	
AT	10,842	18	45	3.5	244.4	244.4	244.7	0.3	
AU	10,952	11	34	4.3	245.4	245.4	245.8	0.4	
AV	11,073	253	1,274	0.1	250.4	250.4	251.1	0.7	
AW	11,228	314	1,569	0.1	250.4	250.4	251.1	0.7	
AX	11,326	58	90	0.8	250.4	250.4	251.1	0.7	
AY	11,434	102	195	1.3	255.4	255.4	256.1	0.7	
AZ	11,558	13	84	1.7	255.5	255.5	256.2	0.7	

<sup>1</sup>Feet above confluence with Beaverton Creek

T,	FEDERAL EMERGENCY MANAGEMENT AGENCY	ΕΙ ΟΟΡΨΑΥ ΠΑΤΑ
B	WASHINGTON COUNTY OR	
G	AND INCORPORATED AREAS	

FLOODING SC	DURCE		FLOODWAY		1-PERCENT-ANNUAL-CHANCE FLOOD WATER SURFACE ELEVATION				
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH	SECTION AREA	MEAN VELOCITY		WITHOUT FLOODWAY	WITH FLOODWAY		
HALL CREEK -		(FEET)	(SQ.FEET)	(FEET/SEC.)	(FEET NAVD)	(FEET NAVD)	(FEET NAVD)	(FEET)	
106TH TRIBUTARY									
Α	138	10	5	4.0	191.6	191.6	191.8	0.2	
В	449	10	5	4.0	195.2	195.2	195.4	0.2	
С	616	10	5	3.9	200.3	200.3	200.5	0.2	
D	766	10	5	4.0	205.2	205.2	205.2	0.0	
Е	912	10	5	4.0	208.4	208.4	208.4	0.0	
F	1.215	7	27	2.6	209.7	209.7	209.9	0.2	
G	1.357	10	20	1.7	209.9	209.9	210.4	0.5	
H	1,507	14	12	2.9	211.9	211.9	211.9	0.0	
1	1,812	7	4	8.0	218.5	218.5	218.5	0.0	
.l	2 162	22	43	0.8	226.1	226.1	226.2	0.1	
ĸ	2,102	10	12	27	231.0	231.0	231.3	0.3	
	2,072	5	17	2.0	231.1	231.0	231.4	0.3	
M	2,400	10	19	1.8	231.7	231.7	237.4	0.0	
N	2,047	3	5	6.9	245.1	245 1	245 1	0.4	
-eet above confluence with Hal	Creek								
FEDERAL EMERG	ENCY MANAGEMENT	AGENCY			FLOOD	WAY DATA			
	ORPORATED ARE	AS		I	HALL CREEK -	106TH TRIBU	TARY		

FLOODING SOURCE		FLOODWAY		1-1	PERCENT-ANNU WATER SURFA	AL-CHANCE FLOC	DD				
CROSS SECTION DISTA	NCE <sup>1</sup> (FEET)	SECTION AREA (SO FEET)	MEAN VELOCITY (EEET/SEC.)	REGULATORY	WITHOUT FLOODWAY (FEET NAVD)	WITH FLOODWAY (FEET NAVD)	INCREASE				
ALL CREEK - NORTH		(OQ.I LLI)	(I LE 1/3EC.)	(ILLINAVD)	(I LET NAVD)	(ILLINAVD)	(1 = 1 )				
FORK A 18 B 47 C 55 D 66 E 80 F 1,2 G 1,4 H 1,5 I 1,6 J 2,0 K 2,1 L 2,2 M 2,3 N 2,7 O 3,0 P 3,2 et above confluence with Hall Creek	32       9         75       30         53       30         58       24         54       13         524       39         524       39         525       10         576       10         599       18         505       30         101       37         245       32         382       43         739       54         956       61         245       62	16 18 78 220 135 300 98 103 166 209 256 244 258 328 231 178	3.2 2.7 0.6 1.1 1.9 0.8 2.4 2.2 1.5 1.4 1.1 1.0 0.9 0.8 0.9 1.3	181.1 181.1 182.3 182.4 182.5 182.5 182.5 182.5 182.5 182.5 182.5 182.6 182.6 182.6 182.6	181.1 182.3 182.4 182.4 182.5 182.5 182.5 182.5 182.5 182.5 182.5 182.6 182.6 182.6 182.6	181.2 181.4 182.4 182.4 182.7 182.7 183.0 183.2 183.3 183.4 183.4 183.4 183.5 183.5 183.5 183.5	0.1 0.3 0.1 0.0 0.2 0.2 0.5 0.7 0.8 0.9 0.9 0.9 0.9 0.9 0.9 1.0				
FEDERAL EMERGENCY MAN	AGEMENT AGENCY			FL OOD	ω ΔΤΔ						
	WASHINGTON COUNTY, OR										

	OURCE		FLOODWAY		1-PERCENT-ANNUAL-CHANCE FLOOD WATER SURFACE ELEVATION				
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH	SECTION AREA	MEAN VELOCITY	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE	
		(FEET)	(SQ.FEET)	(FEET/SEC.)	(FEET NAVD)	(FEET NAVD)	(FEET NAVD)	(FEET)	
HALL CREEK -									
SOUTH FORK									
A	147	27	12	3.9	212.4	212.4	212.4	0.0	
В	378	23	11	4.0	218.1	218.1	218.1	0.0	
С	612	8	22	3.4	218.3	218.3	218.5	0.2	
D	902	30	87	0.9	220.7	220.7	221.0	0.3	
E	1,017	40	56	0.8	221.2	221.2	221.3	0.1	
F	1,161	15	17	2.6	224.2	224.2	224.2	0.0	
G	1,365	42	42	1.0	227.7	227.7	227.8	0.1	
Н	1,764	10	16	2.7	231.3	231.3	231.9	0.6	
Ι	2,088	10	15	2.8	235.1	235.1	235.9	0.8	
J	2,434	30	8	3.0	239.5	239.5	239.6	0.1	
К	2,621	27	52	0.5	241.1	241.1	241.2	0.1	
L	2,747	7	25	2.1	241.8	241.8	242.6	0.8	
Μ	2,852	12	36	1.2	241.9	241.9	242.8	0.9	
Ν	2,999	7	7	5.9	243.1	243.1	243.1	0.0	
0	3,121	17	35	1.2	245.9	245.9	246.6	0.7	
Р	3,258	15	42	1.0	247.9	247.9	248.7	0.8	
Q	3,374	22	16	1.4	249.7	249.7	250.1	0.4	
R	3.534	13	6	3.9	252.1	252.0	252.0	0.0	
S	3,580	22	14	1.7	253.1	253.1	253.1	0.0	
T	3.836	5	4	7.2	258.1	258.1	258.1	0.0	
U	3,990	10	9	3.5	259.8	259.8	259.8	0.0	
V	4.035	22	68	0.4	260.1	260.1	260.1	0.0	

<sup>1</sup>Feet above confluence with Hall Creek

FEDERAL EMERGENCY MANAGEMENT AGENCY WASHINGTON COUNTY, OR AND INCORPORATED AREAS
FLOODWAY DATA
HALL CREEK - SOUTH FORK

FLOODING S	OURCE		FLOODWAY		1-PERCENT-ANNUAL-CHANCE FLOOD WATER SURFACE ELEVATION				
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH	SECTION AREA	MEAN VELOCITY	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE	
		(FEET)	(SQ.FEET)	(FEET/SEC.)	(FEET NAVD)	(FEET NAVD)	(FEET NAVD)	(FEET)	
HEDGES CREEK									
А	823	40	359	1.7	128.9	122.1 <sup>2</sup>	123.0 <sup>2</sup>	0.9	
В	1,384	72	474	1.5	128.9	122.4 <sup>2</sup>	123.3 <sup>2</sup>	0.9	
С	1.442	78	555	0.9	128.9	122.4 <sup>2</sup>	123.3 <sup>2</sup>	0.9	
D	1.895	141	823	0.6	128.9	122.4 <sup>2</sup>	123.3 <sup>2</sup>	0.9	
E	1,998	177	1,017	0.3	128.9	122.4 <sup>2</sup>	123.4 <sup>2</sup>	1.0	
F	2.137	190	1.066	0.3	128.9	122.4 <sup>2</sup>	123.4 <sup>2</sup>	1.0	
G	2.330	188	1.391	0.5	128.9	125.1 <sup>2</sup>	125.9 <sup>2</sup>	0.8	
Н	2.642	205	1.547	0.6	128.9	125.1 <sup>2</sup>	125.9 <sup>2</sup>	0.8	
I	3.164	117	753	1.7	128.9	125.1 <sup>2</sup>	126.0 <sup>2</sup>	0.9	
J	3.267	215	1.171	0.9	128.9	$125.2^{2}$	$126.0^{2}$	0.8	
К	4.288	188	1.122	1.0	128.9	125.7 <sup>2</sup>	$126.2^2$	0.5	
L	4.664	117	562	1.8	128.9	126.7 <sup>2</sup>	127.1 <sup>2</sup>	0.4	
М	5.002	116	623	1.4	128.9	$126.9^{2}$	127.3 <sup>2</sup>	0.4	
Ν	5.577	84	359	2.9	128.9	127.4 <sup>2</sup>	127.8 <sup>2</sup>	0.4	
0	6,148	87	530	1.7	128.9	127.8 <sup>2</sup>	$128.5^{2}$	0.7	
Р	6,681	76	597	2.0	128.9	$128.1^2$	$128.9^2$	0.8	
Q	7,162	66	252	3.5	129.3	129.3	129.7	0.4	
R	7,699	27	152	6.3	133.1	133.1	133.2	0.1	
S	7,918	136	770	1.3	133.9	133.9	134.4	0.5	
Т	8,365	171	1,202	0.8	133.9	133.9	134.5	0.6	
U	8,742	72	495	1.6	133.9	133.9	134.5	0.6	
V	9,353	74	418	1.9	134.4	134.4	134.9	0.5	
W	9,554	61	348	2.3	134.6	134.6	135.1	0.5	
X	10,016	50	133	6.U 2 0	136.1	136.1	136.2	0.1	
т 7	10,959	30 32	294 143	2.0 5.2	139.9	139.9	140.4	0.5	
£	11,010	02	071	0.2	172.1	176.1	172.0	0.7	

<sup>2</sup>Elevations computed without consideration of backwater effects from Tualatin River

FEDERAL EMERGENCY MANAGEMENT AGENCY WASHINGTON COUNTY, OR AND INCORPORATED AREAS FLOODWAY DATA HEDGES CREEK

FLOODING SC	OURCE		FLOODWAY		1-1	PERCENT-ANNU WATER SURFA	AL-CHANCE FLOO	DD
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH (FEET)	SECTION AREA (SQ.FEET)	MEAN VELOCITY (FEET/SEC.)	REGULATORY (FEET NAVD)	WITHOUT FLOODWAY (FEET NAVD)	WITH FLOODWAY (FEET NAVD)	INCREASE (FEET)
HOLCOMB CREEK								
A B C D E F G H I J K L M N O P	207 800 1,476 2,453 2,817 3,105 3,653 4,537 5,445 6,416 7,335 8,277 8,664 9,176 9,724 10,539 k Creek North	71 203 132 64 68 68 59 48 78 98 81 252 307 262 75 19	222 885 632 139 193 180 155 295 205 141 141 148 91 101 78 65 85	2.9 0.6 0.7 5.2 2.6 3.1 3.6 2.7 2.5 3.3 2.3 4.5 2.7 4.0 5.7 3.7	178.3 178.3 178.3 178.3 178.3 178.7 180.2 185.9 186.0 189.5 192.9 198.1 199.9 203.1 207.2 211.5	$175.3^2$ $175.5^2$ $177.7^2$ $178.2^2$ 178.7 180.2 185.9 186.0 189.5 192.9 198.1 199.9 203.1 207.2 211.5	176.2 <sup>2</sup> 176.4 <sup>2</sup> 176.5 <sup>2</sup> 178.3 <sup>2</sup> 179.2 <sup>2</sup> 179.7 181.1 186.8 187.0 190.1 193.8 199.2 200.8 204.1 208.1 211.8	0.9 0.9 1.0 0.6 1.0 0.9 0.9 1.0 0.6 0.9 1.1 0.9 1.0 0.9 0.3
FEDERAL EMERG		AGENCY			FI OOF			
WASHINGT	ON COUNT	Y, OR						

	OURCE		FLOODWAY		1-PERCENT-ANNUAL-CHANCE FLOOD WATER SURFACE ELEVATION				
	1	WIDTH	SECTION	MEAN	REGULATORY	WITHOUT	WITH	INCREASE	
CROSS SECTION	DISTANCE'		AREA	VELOCITY		FLOODWAY	FLOODWAY		
		(FEET)	(SQ.FEET)	(FEET/SEC.)	(FEET NAVD)	(FEET NAVD)	(FEET NAVD)	(FEET)	
McKAY CREEK									
А	2,402	904	4,578	3.2	156.2	144.0 <sup>2</sup>	144.4 <sup>2</sup>	0.4	
В	5,424	904	5,385	2.9	156.2	144.9 <sup>2</sup>	145.6 <sup>2</sup>	0.7	
С	6.713	755	4.047	3.6	156.2	145.5 <sup>2</sup>	146.5 <sup>2</sup>	1.0	
D	7.267	174	1.674	4.7	156.2	$146.6^{2}$	147.5 <sup>2</sup>	0.9	
Е	8,284	324	2.321	4.8	156.2	$148.3^{2}$	149.1 <sup>2</sup>	0.8	
F	9 134	285	2 552	4.8	156.2	$149.2^2$	150 2 <sup>2</sup>	1.0	
G	12 500	120	1,318	7.3	156.2	$152.6^{2}$	153 1 <sup>2</sup>	0.5	
Н	12,000	514	6 106	1.0	156.2	$153.9^2$	154 8 <sup>2</sup>	0.0	
1	13 841	643	7 219	1.6	156.2	$154.0^2$	154 9 <sup>2</sup>	0.0	
	1/ 808	635	6,836	1.0	156.2	154.0	155.02	0.9	
ĸ	17,641	686	5 548	2.7	156.2	154.1	155.0	0.9	
	20.386	307	3 3 3 5	3.4	156.4	156.4	157.1	0.0	
M	21,680	480	4 812	24	156.9	156.9	157.6	0.7	
N	23.639	652	6.149	1.9	157.4	157.4	158.0	0.6	
0	24,798	635	5,002	2.2	158.7	158.7	159.4	0.7	
P	29,941	362	3,400	2.9	160.0	160.0	160.8	0.8	
Q	33,869	465	3,999	2.2	161.4	161.4	162.2	0.8	
R	35,617	202	2,466	3.4	161.9	161.9	162.8	0.9	
S	35,775	96	1,175	4.7	162.0	162.0	163.0	1.0	
Т	35,822	119	1,381	4.7	162.4	162.4	163.2	0.8	
U	37,420	338	3,128	2.7	163.5	163.5	164.4	0.9	
V	38,688	531	4,696	1.9	164.0	164.0	164.8	0.8	
W	45,547	106	1,071	5.0	167.5	167.5	168.4	0.9	
X	45,679	83	1,002	5.4	168.5	168.5	169.2	0.7	
Y Z	40,098	390	3,322	2.3	169.9	169.9	170.0	0.7	
L	40,000	90	000	1.9	170.4	170.4	171.5	0.9	

<sup>1</sup>Feet above confluence with Dairy Creek

<sup>2</sup>Elevations computed without consideration of backwater effects from Dairy Creek

FEDERAL EMERGENCY MANAGEMENT AGENCY WASHINGTON COUNTY, OR AND INCORPORATED AREAS MCKAY CREEK

FLOODING S	OURCE		FLOODWAY		1-	PERCENT-ANNU WATER SURFA	AL-CHANCE FLOG	DD
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH (FEET)	SECTION AREA (SQ.FEET)	MEAN VELOCITY (FEET/SEC.)	REGULATORY (FEET NAVD)	WITHOUT FLOODWAY (FEET NAVD)	WITH FLOODWAY (FEET NAVD)	INCREASE (FEET)
McKAY CREEK				, , , , ,				
AA AB AC AD AE	49,626 52,091 53,646 54,233 54,337	405 409 415 105 223	3,798 3,146 3,427 972 2,103	1.9 2.7 2.2 4.7 3.5	172.5 172.9 173.3 173.6 174.5	172.5 172.9 173.3 173.6 174.5	173.2 173.6 174.1 174.4 175.1	0.7 0.8 0.8 0.6
eet above confluence with Da	ıry Creek							
					FLOOD	WAY DATA		
		11, UK			McKA	AY CREEK		

CROSS SECTION					1-PERCENT-ANNUAL-CHANCE FLOOD WATER SURFACE ELEVATION			
	DISTANCE <sup>1</sup>	WIDTH	SECTION AREA	MEAN VELOCITY	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE
		(FEET)	(SQ.FEET)	(FEET/SEC.)	(FEET NAVD)	(FEET NAVD)	(FEET NAVD)	(FEET)
NORTH JOHNSON								
CREEK								
А	112	45	222	2.4	187.0	187.0	187.0	0.0
В	534	14	119	4.4	187.5	187.5	187.7	0.2
С	680	24	189	2.8	187.9	187.9	188.1	0.2
D	898	26	196	2.7	188.2	188.2	188.4	0.2
E	1,198	41	170	3.9	188.6	188.6	188.8	0.2
F	1,680	36	197	2.7	189.4	189.4	189.6	0.2
G	2,152	27	180	2.9	189.9	189.9	190.2	0.3
Н	3,041	189	1,284	0.3	190.1	190.1	190.7	0.6
I	3,280	204	1,524	0.1	190.1	190.1	190.7	0.6
J	3,884	233	1,230	0.2	190.1	190.1	190.7	0.6
К	4,609	32	129	3.0	190.7	190.7	191.1	0.4
L	4,796	20	176	2.6	196.3	196.3	197.0	0.7
М	4,942	34	272	1.6	196.3	196.3	197.2	0.9
Ν	5,334	35	235	1.8	196.4	196.4	197.3	0.9
0	5,747	57	232	1.8	196.4	196.4	197.4	1.0
Р	6,259	167	264	1.9	198.0	198.0	198.6	0.6
Q	6,560	8	32	11.4	201.7	201.7	201.7	0.0
R	6,814	8	64	5.8	206.4	206.4	206.4	0.0
S	6,913	13	119	3.1	207.1	207.1	207.1	0.0
Т	7,393	41	234	1.4	207.1	207.1	207.7	0.6
U	7,911	49	307	1.4	208.2	208.2	208.9	0.7
V	8,465	193	134	5.5	209.8	209.8	210.4	0.6
W	9,065	110	92	4.4	212.4	212.4	212.7	0.3
х	9,269	152	143	2.2	214.6	214.6	214.6	0.0
Y	10,057	40	79	4.9	218.9	218.9	219.6	0.7
Z	10,520	15	254	1.2	237.0	237.0	237.0	0.0

<sup>1</sup>Feet above confluence with Cedar Mill Creek

	FEDERAL EMERGENCY MANAGEMENT AGENCY	Ţ
PLOODWAT DATA		B
	WASHINGTON COUNTY, OR -	
NORTH JOHNSON CREEK	AND INCORPORATED AREAS	σı
	AND INCORPORATED AREAS	BLE 5

FLOODING SC	DURCE		FLOODWAY		1-1	1-PERCENT-ANNUAL-CHANCE FLOOD WATER SURFACE ELEVATION					
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH	SECTION AREA (SO EEET)	MEAN VELOCITY (EEET/SEC.)		WITHOUT FLOODWAY (FEET NAVD)	WITH FLOODWAY (FEET NAVD)	INCREASE			
				(I LL 1/3LC.)	(ILLINAVD)	(ILLINAVD)	(ILLINAVD)				
CREEK											
AA	10,929	73	465	0.7	237.1	237.1	237.1	0.0			
AB	11,252	29	76	4.0	237.6	237.6	237.8	0.2			
AC	11,657	110	181	1.7	242.1	242.1	242.1	0.0			
AD	12,030	60	90	3.5	245.9	245.9	245.9	0.0			
AE	12,426	110	165	1.9	249.4	249.4	249.4	0.0			
AF	12,613	42	88	3.9	250.7	250.7	250.9	0.2			
AG	12,996	30	84	4.0	254.4	254.4	255.0	0.6			
AH	13.320	21	47	5.5	259.6	259.6	259.8	0.2			
AI	13,770	15	39	7.1	276.4	276.4	277.0	0.6			
AJ	14,136	14	26	6.0	293.6	293.6	293.7	0.1			
AK	14.419	23	30	4.6	306.9	306.9	307.2	0.3			
t above confluence with Cec	lar Mill Creek			1	1		1				
FEDERAL EMERG		AGENCY			FLOOD	WAY DATA					
WASHINGT		ΓY, OR					17				
		۵S		NORTH JOHNSON CREEK							

FLOODING SC	URCE		FLOODWAY			1-PERCENT-ANNUAL-CHANCE FLOOD WATER SURFACE ELEVATION			
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH (FEET)	SECTION AREA (SQ.FEET)	MEAN VELOCITY (FEET/SEC.)	REGULATORY (FEET NAVD)	WITHOUT FLOODWAY (FEET NAVD)	WITH FLOODWAY (FEET NAVD)	INCREASE (FEET)	
NORTH JOHNSON		( )	(	( /	,	,	,	( )	
EAST TRIBUTARY									
A	376	32	15	3.9	252.0	252.0	252.0	0.0	
B	619	8	29	2.0	254.5	254.5	255.3	0.8	
Ċ	921	9	10	5.9	258.8	258.8	258.8	0.0	
D	1 224	16	15	3.8	281.1	281.1	281.1	0.0	
F	1,505	20	21	2.8	290.4	290.4	201.1	0.0	
F	1,909	9	10	5.9	327.1	327.1	327.1	0.0	
NORTH JOHNSON NORTH TRIBUTARY									
А	544	61	31	4.1	222.0	222.0	222.0	0.0	
В	873	37	50	3.0	229.9	229.9	230.0	0.1	
С	1,165	8	37	3.5	237.3	237.3	237.4	0.1	
D	1,338	15	62	2.4	242.7	242.7	242.7	0.0	
E	1,576	15	19	6.6	252.0	252.0	252.0	0.0	
F	1,803	21	57	2.2	255.8	255.8	255.8	0.0	
G	1,981	10	17	7.5	262.5	262.5	262.5	0.0	
Н	2,089	4	31	4.1	270.9	270.9	270.9	0.0	
1	2.603	24	22	6.3	290.2	290.2	290.2	0.0	
J	3,157	7	13	7.8	343.3	343.3	343.3	0.0	
-	-,								
et above confluence with Nort	h Johnson Creek		I	<u> </u>	<u> </u>		<u>  </u>		
FEDERAL EMERG		AGENCY			FLOOD	WAY DATA			
WASHINGT	ON COUNT	Y, OR						DIES	

AND INCORPORATED AREAS

FLOODING SC	DURCE		FLOODWAY		1-1	PERCENT-ANNU WATER SURFA	AL-CHANCE FLOO	
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH <sup>2</sup> (FEET)	SECTION AREA (SQ.FEET)	MEAN VELOCITY (FEET/SEC.)	REGULATORY (FEET NAVD)	WITHOUT FLOODWAY (FEET NAVD)	WITH FLOODWAY (FEET NAVD)	INCREASE (FEET)
NYBERG SLOUGH		. ,					· · · · · ·	. ,
A B C D E F G H I J K <sup>2</sup>	643 755 994 1,593 1,744 2,193 2,926 3,550 3,938 4,219 5,081	504 559 403 146 109 349 393 90 131 226	6,898 6,993 5,518 1,306 1,593 5,407 5,097 5,605 768 1,614 2,108	0.4 0.3 0.5 3.6 2.5 0.3 0.8 0.5 5.7 4.3 1.0	126.0 126.0 126.0 126.6 126.6 126.6 126.6 126.6 127.9 127.9	126.0 126.0 126.0 126.6 126.6 126.6 126.6 126.6 127.9 127.9	126.2 126.3 126.3 126.2 126.9 127.0 127.0 126.9 128.1 128.2	0.2 0.3 0.2 0.3 0.4 0.4 0.4 0.4 0.3 0.2 0.3
nis table shows the Nyberg Slou	ugh in Clakamas County	v and Washington Cou	nty					
FEDERAL EMERG		AGENCY			FLOOD	WAY DATA		
KING C	FOUNIY, W	A AS	NYBEI	RG SLOUGH (I	N WASHINGTO		ND CLAKAMAS	6 COUNTY)

FLOODING SOURCE			FLOODWAY		1-PERCENT-ANNUAL-CHANCE FLOOD WATER SURFACE ELEVATION			
		WIDTH	SECTION	MEAN		WITHOUT	WITH	
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH	AREA	VELOCITY	REGULATORY	FLOODWAY	FLOODWAY	INCREASE
		(FEET)	(SQ.FEET)	(FEET/SEC.)	(FEET NAVD)	(FEET NAVD)	(FEET NAVD)	(FEET)
ROCK CREEK NORTH								
А	1,801	264	2,586	4.1	147.0	135.0 <sup>2</sup>	136.0 <sup>2</sup>	1.0
В	2,680	205	2,542	4.9	147.0	136.0 <sup>2</sup>	136.8 <sup>2</sup>	0.8
С	3,167	194	2,130	6.1	147.0	136.7 <sup>2</sup>	137.5 <sup>2</sup>	0.8
D	3,652	182	2,192	6.1	147.0	137.1 <sup>2</sup>	138.1 <sup>2</sup>	1.0
E	4,131	130	1,674	5.6	147.0	137.6 <sup>2</sup>	138.7 <sup>2</sup>	1.1
F	4,854	196	2,562	4.0	147.0	139.5 <sup>2</sup>	140.3 <sup>2</sup>	0.8
G	6,139	199	2,667	3.5	147.0	140.3 <sup>2</sup>	141.2 <sup>2</sup>	0.9
Н	7,342	158	2,131	5.1	147.0	141.0 <sup>2</sup>	141.9 <sup>2</sup>	0.9
I	7,860	169	2,359	4.8	147.0	142.0 <sup>2</sup>	142.7 <sup>2</sup>	0.7
J	8,444	228	3,025	4.2	147.0	142.1 <sup>2</sup>	143.1 <sup>2</sup>	1.0
К	9,629	324	4,237	2.7	147.0	142.5 <sup>2</sup>	143.5 <sup>2</sup>	1.0
L	12,191	278	3,626	2.8	147.0	143.0 <sup>2</sup>	143.9 <sup>2</sup>	0.9
М	12,943	237	2,933	4.4	147.0	143.1 <sup>2</sup>	144.1 <sup>2</sup>	1.0
Ν	13,574	290	3,527	3.5	147.0	143.4 <sup>2</sup>	144.4 <sup>2</sup>	1.0
0	14,222	290	3,461	3.8	147.0	143.6 <sup>2</sup>	144.6 <sup>2</sup>	1.0
Р	15,554	342	4,275	2.9	147.0	144.0 <sup>2</sup>	144.9 <sup>2</sup>	0.9
Q	16,515	294	3,401	3.6	147.0	144.2 <sup>2</sup>	145.1 <sup>2</sup>	0.9
R	16,792	159	2,205	5.3	147.0	145.2 <sup>2</sup>	145.7 <sup>2</sup>	0.5
S	17,307	285	3,609	3.4	147.0	145.6 <sup>2</sup>	146.1 <sup>2</sup>	0.5
Т	18,596	337	3,940	3.3	147.0	145.9 <sup>2</sup>	146.3 <sup>2</sup>	0.4
U	19,348	289	2,883	4.4	147.0	146.1 <sup>2</sup>	146.6 <sup>2</sup>	0.5
V	19,960	354	3,664	3.4	147.0	146.4 <sup>2</sup>	146.9 <sup>2</sup>	0.5
W	20,736	299	3,177	3.8	147.0	146.7 <sup>2</sup>	147.2 <sup>2</sup>	0.5
Х	21,420	279	3,249	2.9	147.0	146.8 <sup>2</sup>	147.4 <sup>2</sup>	0.6
Y	22,301	332	3,667	2.8	147.0	147.0	147.7	0.7
Z	23,050	475	4,709	3.0	147.2	147.2	147.9	0.7

<sup>2</sup>Elevations computed without consideration of backwater effects from Tualatin River

FEDERAL EMERGENCY MANAGEMENT AGENCY WASHINGTON COUNTY, OR AND INCORPORATED AREAS AND INCORPORATED AREAS

FLOODING SOURCE			FLOODWAY		1-PERCENT-ANNUAL-CHANCE FLOOD WATER SURFACE ELEVATION			
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH	SECTION AREA	MEAN VELOCITY	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE
		(FEET)	(SQ.FEET)	(FEET/SEC.)	(FEET NAVD)	(FEET NAVD)	(FEET NAVD)	(FEET)
ROCK CREEK NORTH								
AA	24,285	510	4,185	3.2	147.3	147.3	148.1	0.8
AB	25,237	322	3,422	3.5	147.7	147.7	148.5	0.8
AC	25,901	314	3,101	4.0	147.9	147.9	148.7	0.8
AD	26,555	262	2,960	3.9	148.3	148.3	148.9	0.6
AE	27,322	333	3,492	3.5	148.6	148.6	149.2	0.6
AF	27,982	319	3,051	3.2	148.8	148.8	149.6	0.8
AG	28,569	311	3,369	2.6	149.2	149.2	149.9	0.7
AH	29,231	316	3,521	2.7	149.3	149.3	150.1	0.8
AI	30,496	182	1,957	1.7	150.2	150.2	151.1	0.9
AJ	31,289	187	1,771	1.6	150.3	150.3	151.2	0.9
AK	32,472	140	1,207	2.4	150.6	150.6	151.4	0.8
AL	32,569	86	781	3.4	150.8	150.8	151.5	0.7
AM	33,632	217	1,697	1.4	151.2	151.2	151.9	0.7
AN	34,811	191	1,220	2.3	151.5	151.5	152.1	0.6
AO	34,933	193	1,229	2.5	151.5	151.5	152.2	0.7
AP	35,540	163	1,107	2.6	151.8	151.8	152.4	0.6
AQ	36,100	81	626	5.0	152.2	152.2	152.8	0.6
AR	36,608	105	876	3.3	152.6	152.6	153.6	1.0
AS	36,845	170	1,181	2.9	152.7	152.7	153.7	1.0
AT	37,890	58	557	4.7	153.3	153.3	154.1	0.8
AU	38,726	121	942	3.5	154.4	154.4	155.1	0.7
AV	39,009	118	967	3.0	154.5	154.5	155.3	0.8
AW	39,491	128	932	3.2	154.9	154.9	155.7	0.8
AX	40,071	138	1,031	2.9	155.3	155.3	156.1	0.8
AY	40,497	150	1,185	2.3	155.5	155.5	156.3	0.8
AZ	41.004	153	949	32	155.6	155.6	156.6	10

,Τ	FEDERAL EMERGENCY MANAGEMENT AGENCY	FLOODWAY DATA			
₿					
	WASHINGTON COUNTY, OR				
5	AND INCORPORATED AREAS	ROCK CREEK NORTH			

FLOODING SC	OURCE		FLOODWAY		1-PERCENT-ANNUAL-CHANCE FLOOD WATER SURFACE ELEVATION			
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH	SECTION AREA	MEAN VELOCITY	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE
		(FEET)	(SQ.FEET)	(FEET/SEC.)	(FEET NAVD)	(FEET NAVD)	(FEET NAVD)	(FEET)
ROCK CREEK NORTH								
BA	41,826	180	1,176	2.5	156.2	156.2	157.2	1.0
BB	42,399	191	1,053	2.8	156.4	156.4	157.4	1.0
BC	43,433	167	968	3.0	157.1	157.1	158.1	1.0
BD	43,494	166	960	3.0	157.1	157.1	158.1	1.0
BE	44,078	127	683	4.2	157.8	157.8	158.6	0.8
BF	44,294	38	404	6.3	158.2	158.2	159.0	0.8
BG	44,929	170	1,098	2.7	159.3	159.3	160.3	1.0
BH	45.210	250	1,608	1.8	159.4	159.4	160.4	1.0
BI	45.511	204	1,381	2.1	160.1	160.1	161.0	0.9
BJ	45.974	192	1,127	2.6	160.2	160.2	161.2	1.0
ВК	46.447	172	952	2.7	160.5	160.5	161.5	1.0
BL	46,971	120	686	4.3	161.0	161.0	161.8	0.8
BM	47,734	146	727	4.3	162.2	162.2	162.9	0.7
BN	48,162	250	1,149	2.6	162.7	162.7	163.5	0.8
во	48,824	200	1,263	2.1	163.2	163.2	163.8	0.6
BP	49,146	300	1,748	1.3	163.9	163.9	164.4	0.5
BQ	49,469	190	622	4.8	164.0	164.0	164.5	0.5
BR	49,684	89	656	4.1	167.5	167.5	168.1	0.6
BS	50,249	111	932	3.1	168.9	168.9	169.4	0.5
BT	50,580	263	1,530	1.8	169.1	169.1	169.6	0.5
BU	50,692	268	1,345	1.8	169.2	169.2	169.9	0.7
BV	51,156	263	1,624	1.3	169.3	169.3	170.0	0.7
BW	51,639	264	1,685	1.2	169.4	169.4	170.1	0.7
BX	52,074	262	1,467	1.5	169.4	169.4	170.2	0.8
BY	52,397	253	1,024	3.1	169.5	169.5	170.3	0.8
BZ	52,907	233	1,042	2.5	169.8	169.8	170.6	0.8
DZ	52,907	200	1,042	2.0	109.0	109.0	170.0	

T.	FEDERAL EMERGENCY MANAGEMENT AGENCY	FLOODWAY DATA			
AB					
l E	WASHINGTON COUNTY, OR				
сл	AND INCORPORATED AREAS	ROCK CREEK NORTH			

	JURGE		FLOODWAY		1-PERCENT-ANNUAL-CHANCE FLOOD WATER SURFACE ELEVATION			
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH	SECTION AREA	MEAN VELOCITY	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE
		(FEET)	(SQ.FEET)	(FEET/SEC.)	(FEET NAVD)	(FEET NAVD)	(FEET NAVD)	(FEET)
ROCK CREEK NORTH								
CA	53,015	190	882	2.9	170.0	170.0	170.8	0.8
СВ	53,916	109	626	4.5	170.6	170.6	171.5	0.9
CC	54,557	77	500	4.8	172.1	172.1	172.6	0.5
CD	54,787	61	383	6.7	172.6	172.6	173.2	0.6
CE	56,122	67	597	3.5	176.3	176.3	177.2	0.9
CF	57,202	110	814	2.9	177.7	177.7	178.4	0.7
CG	57,448	313	2352	1.1	178.2	178.2	179.1	0.9
СН	58,279	335	2384	1.0	178.3	178.3	179.1	0.9
CI	59,447	435	2644	0.9	178.3	178.3	179.2	0.9
CJ	60,194	510	2383	1.3	178.3	178.3	179.3	1.0
СК	61,015	870	3210	0.5	178.4	178.4	179.3	0.9
CL	62,388	593	1303	1.3	178.4	178.4	179.4	1.0
CM	64,142	169	365	5.0	181.4	181.4	181.5	0.1
CN	65,206	82	350	2.6	184.1	184.1	184.3	0.2
CO	65,969	432	1060	1.7	185.5	185.5	186.0	0.5
CP	66,713	702	725	3.6	186.2	186.2	187.2	1.0
CQ	68,130	220	690	2.4	189.1	189.1	190.0	0.9
CR	69,186	87	299	5.8	191.1	191.1	192.0	0.9
CS	69,972	198	526	3.8	194.0	194.0	194.9	0.9
СТ	70,736	336	935	1.1	195.0	195.0	195.7	0.7
CU	71,262	26	193	5.5	195.8	195.8	196.4	0.6
CV	72,384	226	527	2.7	198.7	198.7	199.1	0.4
CW	72,943	115	289	4.9	199.7	199.7	200.2	0.5
CX	74,073	186	514	3.0	202.3	202.3	202.8	0.5
CY	75,339	290	463	3.4	204.8	204.8	204.9	0.1
CZ	76,654	105	359	3.5	206.7	206.7	207.3	0.6

Ţ	FEDERAL EMERGENCY MANAGEMENT AGENCY	FLOODWAY DATA			
B					
	WASHINGTON COUNTY, OR	ROCK CREEK NORTH			
5	AND INCORPORATED AREAS				

FLOODING S	DURCE		FLOODWAY		1-1	PERCENT-ANNU WATER SURFA	AL-CHANCE FLOO	DD
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH (EEET)	SECTION AREA (SO FEET)	MEAN VELOCITY (FEET/SEC.)	REGULATORY	WITHOUT FLOODWAY (FEET NAVD)	WITH FLOODWAY (FEET NAVD)	INCREASE
ROCK CREEK NORTH		(1221)		(1221/020.)				(1 22 1)
DA DB DC DD DE DF DG DH DI DJ DK DL DM	77,165 77,983 79,349 80,907 81,790 83,164 84,509 84,692 86,000 86,763 87,401 87,916 88,425	188 32 308 323 188 243 50 39 100 26 30 20 16	545 149 512 505 184 500 184 192 204 113 81 111 104	2.3 6.3 2.7 2.3 6.4 2.2 4.9 4.0 4.0 6.5 8.7 6.8 6.5	207.1 209.7 213.5 216.1 219.2 223.4 226.7 227.8 230.6 235.2 237.7 243.9 247.2	207.1 209.7 213.5 216.1 219.2 223.4 226.7 227.8 230.6 235.2 237.7 243.9 247.2	208.0 209.7 214.3 216.7 220.0 224.2 226.8 227.9 230.7 235.2 238.0 243.9 247.4	0.9 0.0 0.8 0.6 0.8 0.1 0.1 0.1 0.1 0.0 0.3 0.0 0.2
FEDERAL EMERG		AGENCY			FLOOD	WAY DATA		
	ON COUN	FY, OR			ROCK C	REEK NORTH		

FLOODING SO	URCE		FLOODWAY		1-1	PERCENT-ANNU/ WATER SURFA	AL-CHANCE FLOO	DD	
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH (FEET)	SECTION AREA (SQ.FEET)	MEAN VELOCITY (FEET/SEC.)	REGULATORY (FEET NAVD)	WITHOUT FLOODWAY (FEET NAVD)	WITH FLOODWAY (FEET NAVD)	INCREASE (FEET)	
ROCK CREEK SOUTH									
A B C D E F G H I J K L M N O P Q	1,478 1,985 2,473 2,688 3,583 4,716 5,036 6,297 7,030 7,710 7,917 8,242 8,907 9,096 10,139 10,613 10,739 atin River	50 61 36 67 50 40 55 35 33 35 37 37 66 33 88 35 31	326 655 297 568 436 350 401 158 121 106 118 194 361 247 626 231 227	2.3 0.8 2.5 1.5 1.0 1.6 1.2 3.3 3.7 4.4 3.3 2.0 1.8 3.1 1.1 2.7 3.1	134.3 134.3 134.3 134.3 134.3 134.3 134.3 134.3 134.3 134.3 134.3 136.9 137.8 138.3 138.4 138.6	$120.1^{2}$ $120.1^{2}$ $120.5^{2}$ $120.7^{2}$ $120.9^{2}$ $121.0^{2}$ $125.1^{2}$ $130.8^{2}$ $132.1^{2}$ $136.3$ $136.9$ $137.8$ $138.3$ $138.4$ $138.6$	$120.9^{2}$ $121.1^{2}$ $121.4^{2}$ $121.6^{2}$ $121.8^{2}$ $122.6^{2}$ $125.7^{2}$ $130.9^{2}$ $132.1^{2}$ $136.4$ $137.1$ $138.0$ $138.5$ $138.7$ $139.0$	0.8 1.0 1.0 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0	
			FLOODWAY DATA						
		T, UK			ROCK CI	REEK SOUTH			

FLOODING S	OURCE		FLOODWAY		1-PERCENT-ANNUAL-CHANGE FLOOD WATER SURFACE ELEVATION				
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH	SECTION AREA	MEAN VELOCITY	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE	
		(FEET)	(SQ.FEET)	(FEET/SEC.)	(FEET NAVD)	(FEET NAVD)	(FEET NAVD)	(FEET)	
SOUTH JOHNSON									
CREEK						_			
A	304	175	531	1.5	171.9	166.1 <sup>2</sup>	166.7 <sup>2</sup>	0.6	
В	616	48	107	9.0	171.9	167.2 <sup>2</sup>	167.3 <sup>2</sup>	0.1	
С	928	24	163	4.9	172.6	172.6	173.1	0.5	
D	1,047	52	393	2.7	173.5	173.5	173.9	0.4	
Е	1,508	90	640	1.6	173.6	173.6	174.1	0.5	
F	2,037	86	556	1.6	173.7	173.7	174.3	0.6	
G	2,520	87	543	1.7	173.7	173.7	174.5	0.8	
Н	2,826	92	591	1.4	173.8	173.8	174.6	0.8	
I	3,100	88	677	1.2	176.1	176.1	176.9	0.8	
J	3,599	78	543	2.0	176.2	176.2	177.1	0.9	
K	3,961	89	564	1.8	176.4	176.4	177.3	0.9	
L	4,254	77	509	1.9	176.6	176.6	177.6	1.0	
М	4,696	103	561	1.8	177.0	177.0	177.9	0.9	
Ν	4,923	81	553	1.5	177.2	177.2	178.1	0.9	
0	5,405	103	580	1.5	177.4	177.4	178.4	1.0	
Р	5,694	68	481	1.9	179.4	179.4	180.2	0.8	
Q	5,954	58	405	2.0	179.4	179.4	180.3	0.9	
R	6,327	47	283	2.6	179.6	179.6	180.5	0.9	
S	6,506	57	355	1.7	180.5	180.5	181.3	0.8	
Т	6,631	55	323	2.2	180.5	180.5	181.4	0.9	
U	6,869	47	263	2.7	180.7	180.7	181.5	0.8	
V	7,155	57	398	1.7	180.9	180.9	181.8	0.9	
W	7,411	71	420	1.5	181.0	181.0	181.9	0.9	
Х	7,646	28	141	4.5	181.9	181.9	182.4	0.5	
Y	8,176	35	226	2.8	183.3	183.3	184.0	0.7	
Z	8,326	35	273	2.3	183.4	183.4	184.3	0.9	

<sup>1</sup>Feet above confluence with Beaverton Creek

<sup>2</sup>Elevations computed without consideration of backwater effects from Beaverton Creek

ТАВ		FLOODWAY DATA
LE 5	AND INCORPORATED AREAS	SOUTH JOHNSON CREEK

FLOODING SC	DURCE		FLOODWAY		1-PERCENT-ANNUAL-CHANCE FLOOD WATER SURFACE ELEVATION			
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH	SECTION AREA	MEAN VELOCITY		WITHOUT FLOODWAY	WITH FLOODWAY	
		(FEET)	(SQ.FEET)	(FEET/SEC.)	(FEET NAVD)	(FEET NAVD)	(FEET NAVD)	(FEET)
CREEK AA AB	8,827 9,166	65 69	266 243	2.8 2.6	184.3 185.1	184.3 185.1	185.2 186.0	0.9 0.9
AC AD	9,349 9,830 10,270	54 60	262 196	2.4 3.6	185.6 187.0 100.1	185.6 187.0 100.1	186.6 188.0 101.0	1.0 1.0
AE AF AG	10,279 10,649 10,929	40 50 55	143 189 171	4.4 3.3 3.7	190.1 192.5 193.9	190.1 192.5 193.9	191.0 193.5 194.9	0.9 1.0 1.0
AH AI AJ	11,267 11,357 11,730	21 75 30	56 429 136	9.2 1.2 4.3	205.3 208.3 215.4	205.3 208.3 215.4	205.3 208.4 215.8	0.0 0.1 0.4
AK AL	12,096 12,352	34 48	165 153	2.9 3.3	218.2 218.6	218.2 218.6	218.7 219.6	0.5 1.0
above confluence with Bea	verton Creek							
					FLOOD	WAY DATA		
		11, UK			SOUTH JO	HNSON CREE	ĸ	

CROSS SECTION         DISTANCE <sup>1</sup> WIDTH (FEET)         SECTION AREA (SQ.FEET)         MEAN VELOCITY (FEET NAVD)         REGULATORY (FEET NAVD)         WITH UT FLOODWAY (FEET NAVD)         WITH FLOODWAY (FEET NAVD)         W	FLOODING S	OURCE		FLOODWAY		1-1	PERCENT-ANNU WATER SURFA	AL-CHANCE FLOO	DD
STOREY CREEK         A         269         105         358         2.1         163.9         163.9         164.7           B         766         124         307         2.2         164.2         166.3         166.3         166.0           D         2,589         87         597         1.4         172.4         173.2         173.4           F         4,460         15         66         7.5         172.8         172.8         173.4           G         4,776         7         66         2.7.9         178.6         178.6         178.7           H         5,543         35         2.58         1.9         180.3         180.3         181.0           J         7,967         31         90         3.6         187.5         187.5         188.5           K         9,467         22         59         5.4         193.1         193.1         193.7         197.8           L         10,349         22         76         3.9         197.4         197.4         197.8	CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH (FEET)	SECTION AREA (SQ.FEET)	MEAN VELOCITY (FEET/SEC.)	REGULATORY (FEET NAVD)	WITHOUT FLOODWAY (FEET NAVD)	WITH FLOODWAY (FEET NAVD)	INCREASE (FEET)
A       269       105       358       2.1       163.9       163.9       164.7         B       766       124       307       2.2       164.2       164.2       165.0         D       2,589       87       597       1.4       172.4       172.4       173.2         E       3,788       142       435       1.1       172.5       172.4       173.4         G       4,776       7       62       7.9       178.6       178.6       178.7         H       5,843       35       258       1.9       180.3       180.3       181.5         J       7,014       12       31       9.3       181.5       181.5       181.5         J       7,967       31       90       3.6       187.5       188.5       188.5         L       10,349       22       76       3.9       197.4       197.4       197.8         L       10,349       22       76       3.9       197.4       197.4       197.8         L       10,349       22       76       3.9       197.4       197.4       197.8         L       10,349       22       76       3.9	STOREY CREEK		, , , , , , , , , , , , , , , , , , ,				, ,	· · · · · · · · · · · · · · · · · · ·	. ,
FEDERAL EMERGENCY MANAGEMENT AGENCY	A B C D E F G H I J K L	269 766 1,727 2,589 3,788 4,460 4,776 5,843 7,014 7,967 9,467 10,349	105 124 67 87 142 15 7 35 12 31 22 22	358 307 167 597 435 66 62 258 31 90 59 76	2.1 2.2 3.6 1.4 1.1 7.5 7.9 1.9 9.3 3.6 5.4 3.9	163.9 164.2 166.3 172.4 172.5 172.8 178.6 180.3 181.5 187.5 193.1 197.4	163.9 164.2 166.3 172.4 172.5 172.8 178.6 180.3 181.5 187.5 193.1 197.4	164.7 165.0 167.0 173.2 173.4 173.4 178.7 181.0 181.5 188.5 193.7 197.8	0.8 0.8 0.7 0.8 0.9 0.6 0.1 0.7 0.0 1.0 0.6 0.4
FLOODWAY DATA	FEDERAL EMERG	ENCY MANAGEMENT	AGENCY						
WASHINGTON COUNTY, OR	WASHING		ΓY, OR			FLOOD	OWAY DATA		

FLOODING SO	URCE		FLOODWAY		1-PERCENT-ANNUAL-CHANCE FLOOD WATER SURFACE ELEVATION			
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH	SECTION AREA (SO FEET)	MEAN VELOCITY (FEET/SEC.)	REGULATORY	WITHOUT FLOODWAY (FEET NAVD)	WITH FLOODWAY (FEET NAVD)	INCREASE
STOREY CREEK FAST		(1 LL1)	(00.1 LL1)	(1 221/320.)			(ILLINAVD)	
TRIBUTARY								
А	1,478	21	30	6.9	174.0	174.0	174.0	0.0
В	2,489	72	477	0.4	184.7	184.7	184.7	0.0
С	3,701	17	61	2.6	185.7	185.7	186.0	0.3
D	4,398	14	31	5.4	187.9	187.9	188.0	0.1
STOREY CREEK MIDDLE TRIBUTARY								
A	806	14	46	5.1	180.2	180.2	181.2	1.0
В	1,041	18	56	3.1	181.7	181.7	182.4	0.7
С	1,741	44	58	4.0	184.7	184.7	184.7	0.0
D	1,861	20	93	1.9	186.0	186.0	186.6	0.6
E	3,103	12	23	8.1	188.9	188.9	188.9	0.0
F	4,063	31	119	1.8	196.0	196.0	196.8	0.8
eet above confluence with Store	ey Creek							
					FLOOD	WAY DATA		
	RPORATED ARE	AS		STOREY	CREEK - EAST	AND MIDDLE	TRIBUTARIES	

FLOODING SC	DURCE		FLOODWAY		1-1	PERCENT-ANNU WATER SURFA	AL-CHANCE FLOO	DD
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH (FEET)	SECTION AREA (SQ.FEET)	MEAN VELOCITY (FEET/SEC.)	REGULATORY (FEET NAVD)	WITHOUT FLOODWAY (FEET NAVD)	WITH FLOODWAY (FEET NAVD)	INCREASE (FEET)
SUMMER CREEK								, ,
A B C D E F G H I J K L M N O P Q	0.02 0.09 0.17 0.40 0.80 1.19 1.23 1.28 1.32 1.36 1.45 1.56 1.70 1.75 1.93 1.97 2.10	161 66 46 101 191 186 186 186 186 65 48 101 61 126 111 86	1,365 385 369 528 922 1,457 1,827 1,803 1,995 1,532 238 269 542 322 553 498 445	1.1 3.8 3.9 2.7 1.6 0.9 0.7 0.7 0.7 0.9 5.6 4.7 2.4 3.7 2.2 2.4 2.7	161.2 161.7 163.8 167.1 173.6 173.7 173.7 173.7 173.6 175.2 175.8 177.1 178.1 178.4 180.3	159.9 <sup>2</sup> 159.9 <sup>2</sup> 161.7 163.8 167.1 173.6 173.7 173.7 173.7 175.2 175.8 177.1 178.1 178.1 178.4 180.3	$160.3^2$ 162.7 164.7 167.6 174.5 174.5 174.6 174.7 174.6 175.8 176.6 177.6 179.0 179.4 181.3	$\begin{array}{c} 0.4\\ 0.4\\ 1.0\\ 0.9\\ 0.5\\ 0.9\\ 0.9\\ 1.0\\ 1.0\\ 1.0\\ 0.6\\ 0.8\\ 0.5\\ 0.9\\ 1.0\\ 1.0\\ 1.0\\ 1.0\\ \end{array}$
FEDERAL EMERG		AGENCY	1		FI OOD			
WASHINGT	ON COUNT	ſY, OR						

FLOODING SC	DURCE		FLOODWAY		1-	PERCENT-ANNU WATER SURFA	AL-CHANCE FLOC	DD
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH <sup>2</sup>	SECTION AREA	MEAN VELOCITY	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE
		(FEET)	(SQ.FEET)	(FEET/SEC.)	(FEET NAVD)	(FEET NAVD)	(FEET NAVD)	(FEET)
TUALATIN RIVER								
AC AD AE AF	35,845 37,920 38,516 40,752	250/410 284/509 253/446 126/380	1,359 446 659 895	5.5 6.3 6.4 5.9	125.0 125.3 125.5 125.9	125.0 125.3 125.5 125.9	125.1 125.4 125.5 126.1	0.1 0.0 0.2
<sup>1</sup> Feet above confluence with Will	amette River							
<sup>2</sup> Eloodway width within City of T	ualatin/Total floodway w	idth						
This FWDT shows the Tualatin F	River reach within city of	Tualalatin in Clakamas	County					
FEDERAL EMERG	ENCY MANAGEMENT	AGENCY			FLOOD	WAY DATA		
	ON COUN	FY, OR AS	TUAL	ATIN RIVER (V		F TUALATIN IN	WASHINGTON	N COUNTY)

FLOODING S	OURCE		FLOODWAY		WATER SURFACE ELEVATION				
			SECTION	MEAN		WITHOUT	WITH		
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH	AREA	VELOCITY	REGULATORY	FLOODWAY	FLOODWAY	INCREASE	
		(FEET)	(SQ.FEET)	(FEET/SEC.)	(FEET NAVD)	(FEET NAVD)	(FEET NAVD)	(FEET)	
TUALATIN RIVER									
А	41,903	255/392 <sup>2</sup>	5,412	6.6	126.3	126.3	126.6	0.3	
В	42,412	102/208 <sup>2</sup>	4,425	7.6	126.6	126.6	126.9	0.3	
С	42,588	200	4,446	7.8	126.8	126.8	127.2	0.4	
D	43,443	374	6,532	5.3	127.9	127.9	128.6	0.7	
E	44,042	419	5,825	6.0	128.3	128.3	129.0	0.7	
F	44,631	286	6,050	5.5	128.9	128.9	129.6	0.7	
G	45,713	235	5,458	6.3	129.1	129.1	129.9	0.8	
Н	46,125	586	8,671	3.9	129.7	129.7	130.6	0.9	
I	46,325	609	8,920	4.3	129.7	129.7	130.6	0.9	
J	47,537	638	8,638	4.4	130.2	130.2	131.1	0.9	
K	47,907	555	8,688	4.3	130.4	130.4	131.3	0.9	
L	48,547	1,038	17,752	1.8	130.8	130.8	131.7	0.9	
Μ	51,159	1,308	20,386	2.3	131.0	131.0	131.9	0.9	
Ν	53,386	1,290	16,561	3.2	131.1	131.1	132.1	1.0	
0	55,226	1,335	20,165	1.5	131.5	131.5	132.5	1.0	
Р	59,644	498	10,118	3.9	132.4	132.4	133.3	0.9	
Q	60,256	384	10,395	3.1	132.8	132.8	133.7	0.9	
R	60,906	589	10,774	3.6	132.9	132.9	133.8	0.9	
S	64,281	711	12,200	3.4	133.4	133.4	134.3	0.9	
Т	65,552	763	13,107	2.8	133.7	133.7	134.6	0.9	
U	68,762	1,583	28,462	1.1	134.1	134.1	135.0	0.9	
V	69,084	1,774	30,924	1.4	134.1	134.1	135.0	0.9	
W	71,178	3,154	50,166	0.8	134.2	134.2	135.0	0.8	
Х	75,994	3,768	50,759	1.3	134.2	134.2	135.1	0.9	
Y	80,096	3,862	52,093	0.5	134.3	134.3	135.2	0.9	
Z	80,604	3,398	46,024	0.7	134.3	134.3	135.2	0.9	

<sup>2</sup>Floodway width within City of Tualatin/Total floodway width

TAB		FLOODWAY DATA
LE 5	AND INCORPORATED AREAS	TUALATIN RIVER

FLOODING S	OURCE		FLOODWAY		1-PERCENT-ANNUAL-CHANCE FLOOD WATER SURFACE ELEVATION				
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH	SECTION AREA	MEAN VELOCITY	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE	
		(FEET)	(SQ.FEET)	(FEET/SEC.)	(FEET NAVD)	(FEET NAVD)	(FEET NAVD)	(FEET)	
TUALATIN RIVER									
AA	82,845	2,528	34,746	0.8	134.4	134.4	135.2	0.8	
AB	83,267	2,483	33,631	1.1	134.4	134.4	135.3	0.9	
AC	84,848	1,681	22,437	2.1	134.4	134.4	135.4	1.0	
AD	85,487	792	9,994	3.0	134.6	134.6	135.5	0.9	
AE	85,696	1,058	15,927	2.3	134.8	134.8	135.8	1.0	
AF	86,585	846	15,373	2.4	135.1	135.1	136.0	0.9	
$AG^4$	189,211	1,859	21,962	1.5	144.3	141.6 <sup>3</sup>	142.5 <sup>3</sup>	0.9	
AH	189,986	1,640	18,134	1.9	144.3	141.7 <sup>3</sup>	142.6 <sup>3</sup>	0.9	
AI	190,800	1,424	16,228	2.2	144.3	141.9 <sup>3</sup>	142.8 <sup>3</sup>	0.9	
AJ	192,431	1,760	22,170	1.4	144.3/144.3 <sup>2</sup>	142.5 <sup>3</sup>	143.4 <sup>3</sup>	0.9	
AK	193.436	2.289	24.940	1.4	144.8/144.3 <sup>2</sup>	142.7 <sup>3</sup>	143.5 <sup>3</sup>	0.8	
AL	196,851	1,941	20,385	1.7	145.6	143.2	144.0	0.8	
AM	198,810	1,626	21,928	1.4	145.7	143.4	144.2	0.8	
AN	200,975	1,278	16,681	2.0	146.2/146.1 <sup>2</sup>	143.9	144.7	0.8	
AO	201.438	1.208	14.856	2.5	146.2/146.2 <sup>2</sup>	144.0	144.8	0.8	
AP	201.868	1.089	13.267	2.8	146.4/146.3 <sup>2</sup>	144.2	145.0	0.8	
AQ	203.771	1.223	17.092	2.1	146.9/146.8 <sup>2</sup>	145.0	145.8	0.8	
AR	204,855	1,188	18.094	1.6	$147.1/146.9^2$	145.3	146.1	0.8	
AS	206.088	533	9,683	3.4	147.5	145.8	146.6	0.8	
AT	207,184	1,298	15,646	2.3	147.9	146.3	147.1	0.8	
AU	208,622	1,602	22,317	1.6	148.2	146.6	147.4	0.8	
AV	209,541	974	15,152	2.1	148.3	146.8	147.5	0.7	
AW	210,609	1,865	23,939	1.4	148.5	147.0	147.7	0.7	
AX	211,885	1,807	27,553	1.3	148.5	147.1	147.8	0.7	
AY	212,955	2,237	30,875	1.2	148.6	147.2	147.8	0.6	
AZ	214,791	2,579	34,801	1.1	148.6	147.2	147.9	0.7	

<sup>1</sup>Feet above confluence with Willamette River

<sup>2</sup>Riverward of levees / Landward of levees

TABLE 5

<sup>3</sup>Elevations computed without consideration of effective water surface elevations downstream of detailed study limit.

<sup>4</sup>Break in detailed study reach between this and previous (downstream) reach

FEDERAL EMERGENCY MANAGEMENT AGENCY

WASHINGTON COUNTY, OR AND INCORPORATED AREAS **FLOODWAY DATA** 

**TUALATIN RIVER**